

An Introduction to X-Analysis Integration (XAI)

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Georgia Tech

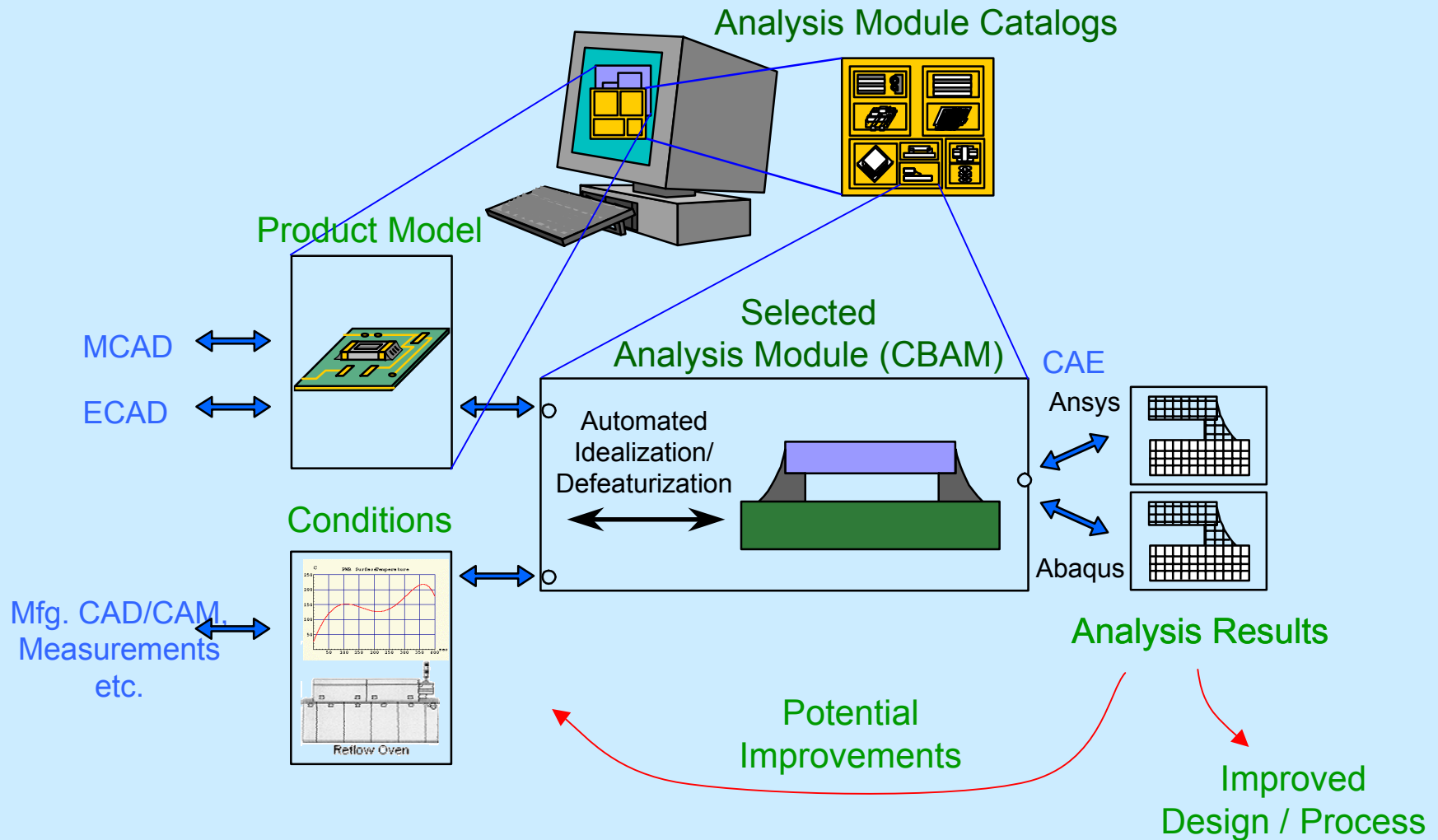
Engineering Information Systems Lab

eislab.gatech.edu

Outline

- ◆ Analysis Integration Challenges
- ◆ Introduction to Constrained Objects (COBs)
- ◆ Overview of COB-based XAI
- ◆ Example Applications
 - ◆ Electronic Packaging Thermomechanical Analysis
 - ◆ Aerospace Structural Analysis
- ◆ Summary

Analysis Integration Thrust



X-Analysis Integration

(X=Design, Mfg., etc.)

◆ Goal:

Improve product engineering processes by integrating analysis models with other life cycle models

◆ Challenges:

- Heterogeneous Transformations
- Diversity: CAD/CAM/CAX Models, Disciplines, Fidelity, Tools, etc.

◆ One Approach:

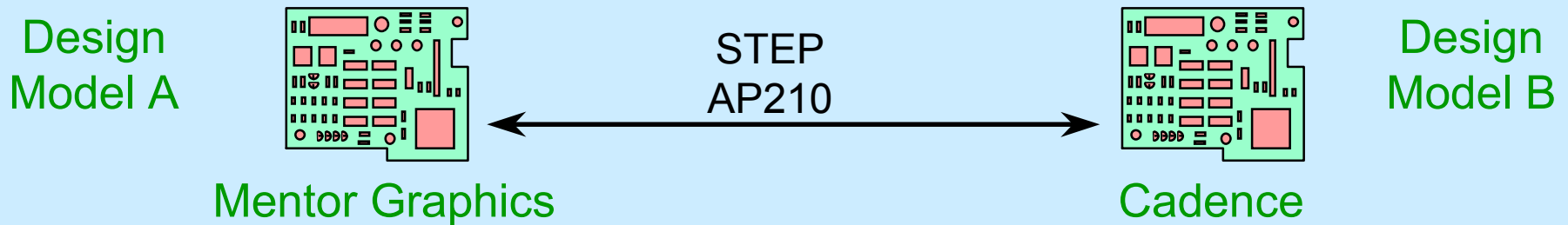
The Multi-Representation Architecture (MRA)

◆ Initial Focus:

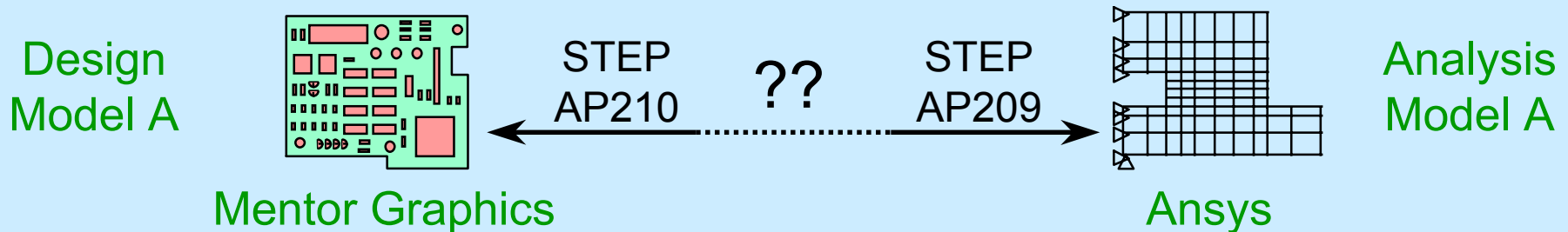
Automation of routine analysis for design

Analysis Integration Challenges: Heterogeneous Transformations

◆ Homogeneous Transformation



◆ Heterogeneous Transformation

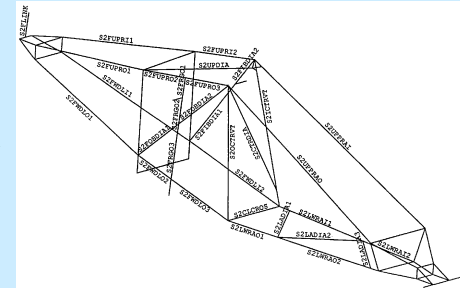


Multifidelity Analysis

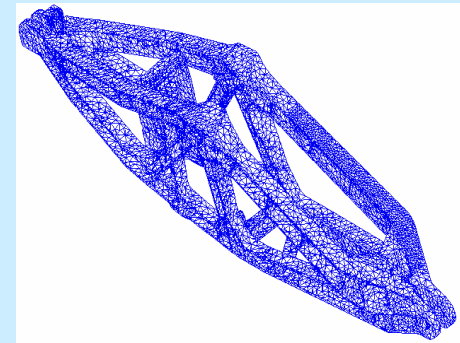
Design Model (MCAD)

Analysis Models (MCAE)

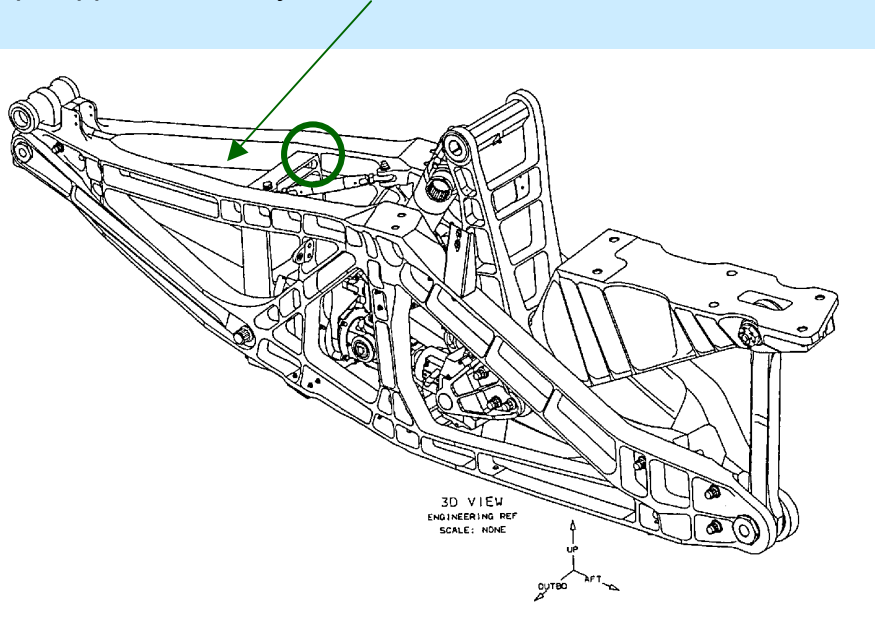
1D Beam/Stick Model



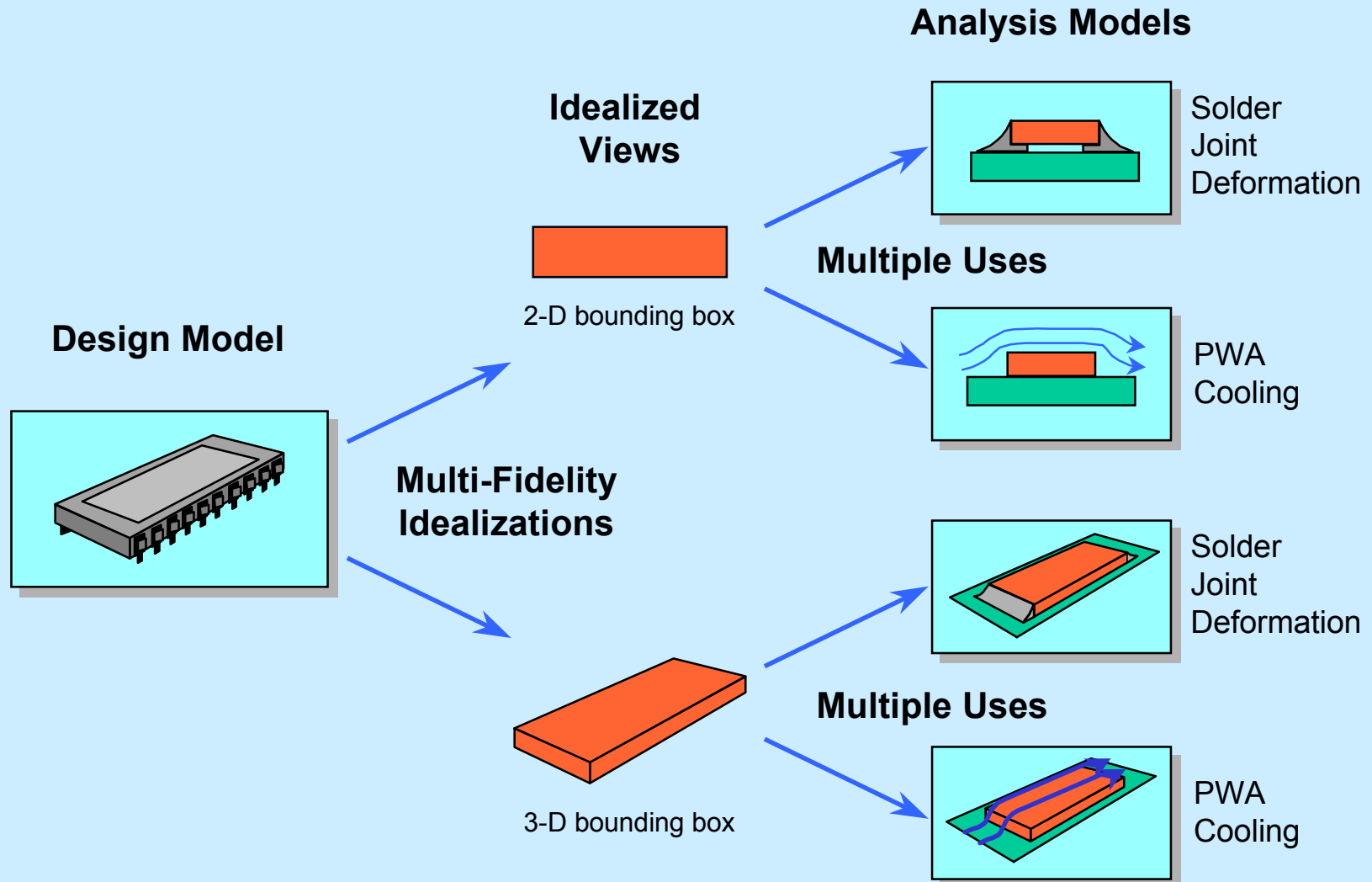
3D Continuum/Brick Model



flap support assembly inboard beam

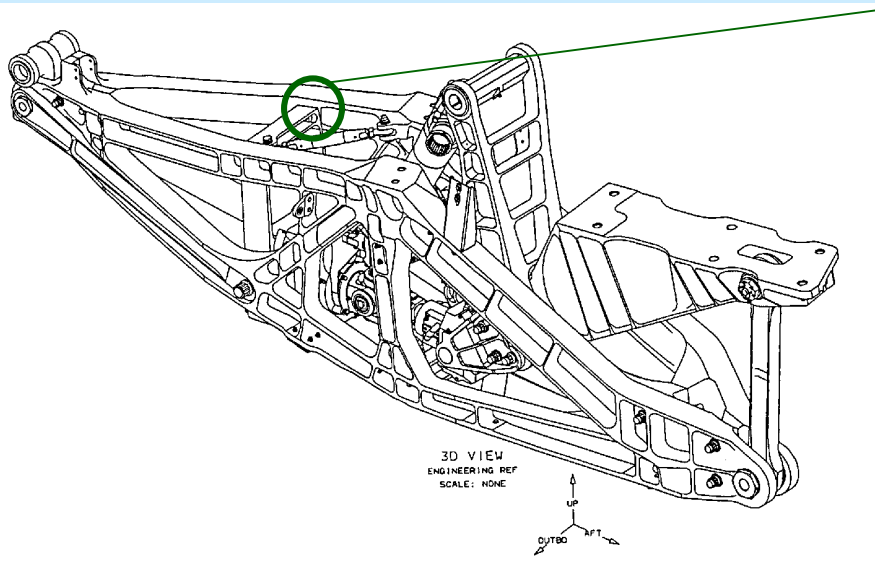


Multi-Fidelity, Multi-Usage Idealizations



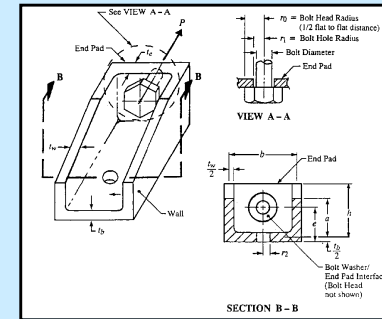
Multilevel Analysis

Design Model (MCAD)

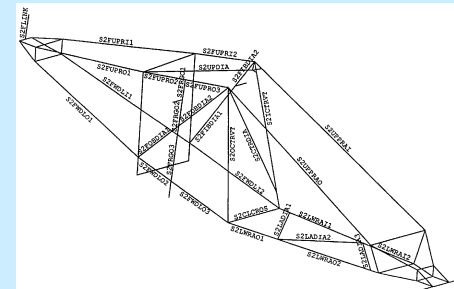


Analysis Models (MCAE)

Part Feature Level Model

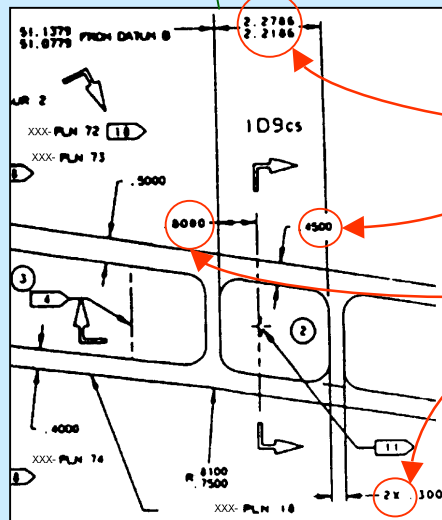
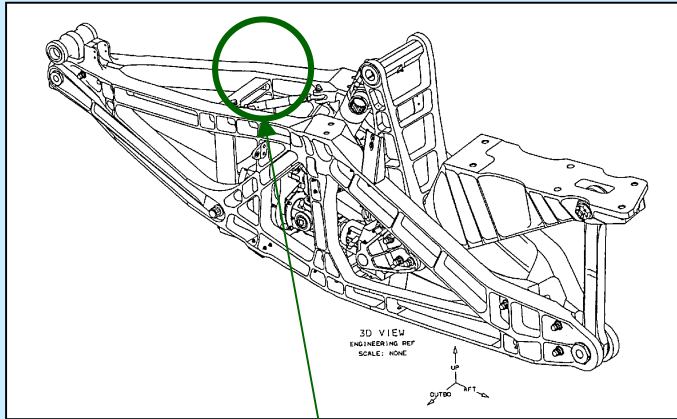


Assembly Level Model

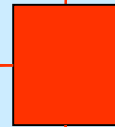


Design Geometry - Analysis Geometry Mismatch

Detailed Design Model

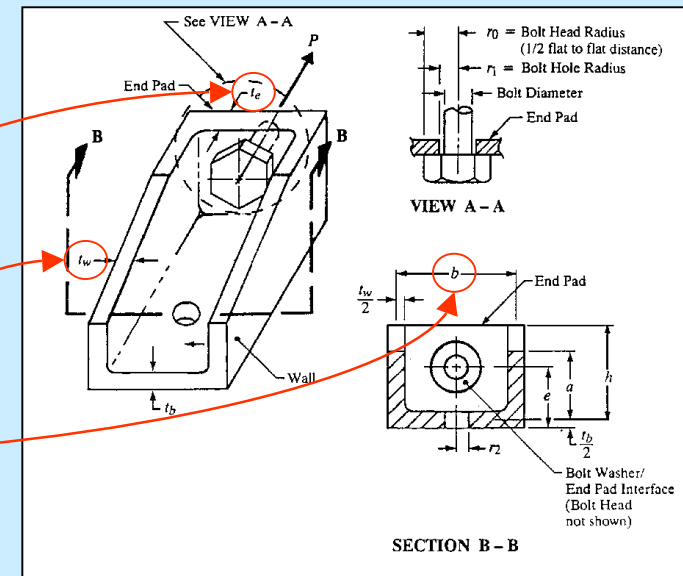


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Idealizations

Analysis Model (with Idealized Features)



Tension Fitting Analysis

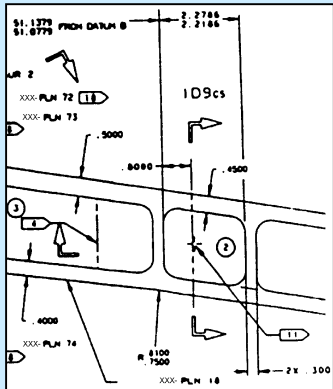
“It is no secret that CAD models are driving more of today’s product development processes ... With the growing number of design tools on the market, however, the interoperability gap with downstream applications, such as finite element analysis, is a very real problem. As a result, CAD models are being recreated at unprecedented levels.”

Ansys/ITI press Release, July 6 1999

<http://www.ansys.com/webdocs/VisitAnsys/CorpInfo/PR/pr-060799.html>

Explicit Design-Analysis Associativity

bulkhead assembly attach point
CAD model



*Missing
CAD-CAE
associativity*

material properties
idealized geometric attributes

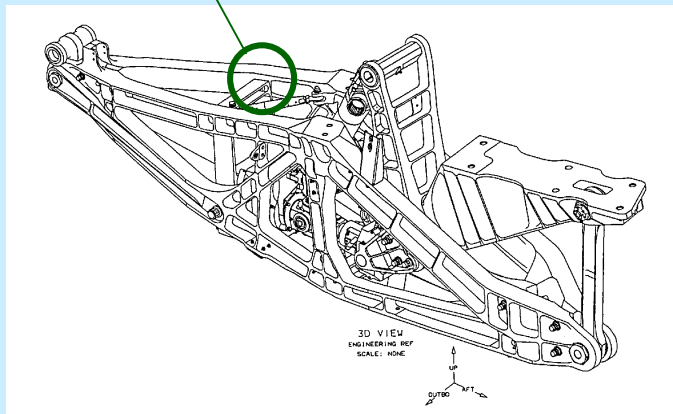
analysis results

channel fitting analysis

LINKAGE SUPPORT NO. 2 (INBOARD BEAM REF 123L4567)
Bulkhead Assembly Attach Point at Upper Beam Location

BATHTUB TYPE TENSION FITTING ANALYSIS
REF:DM6-81766, "Tension-type fittings"

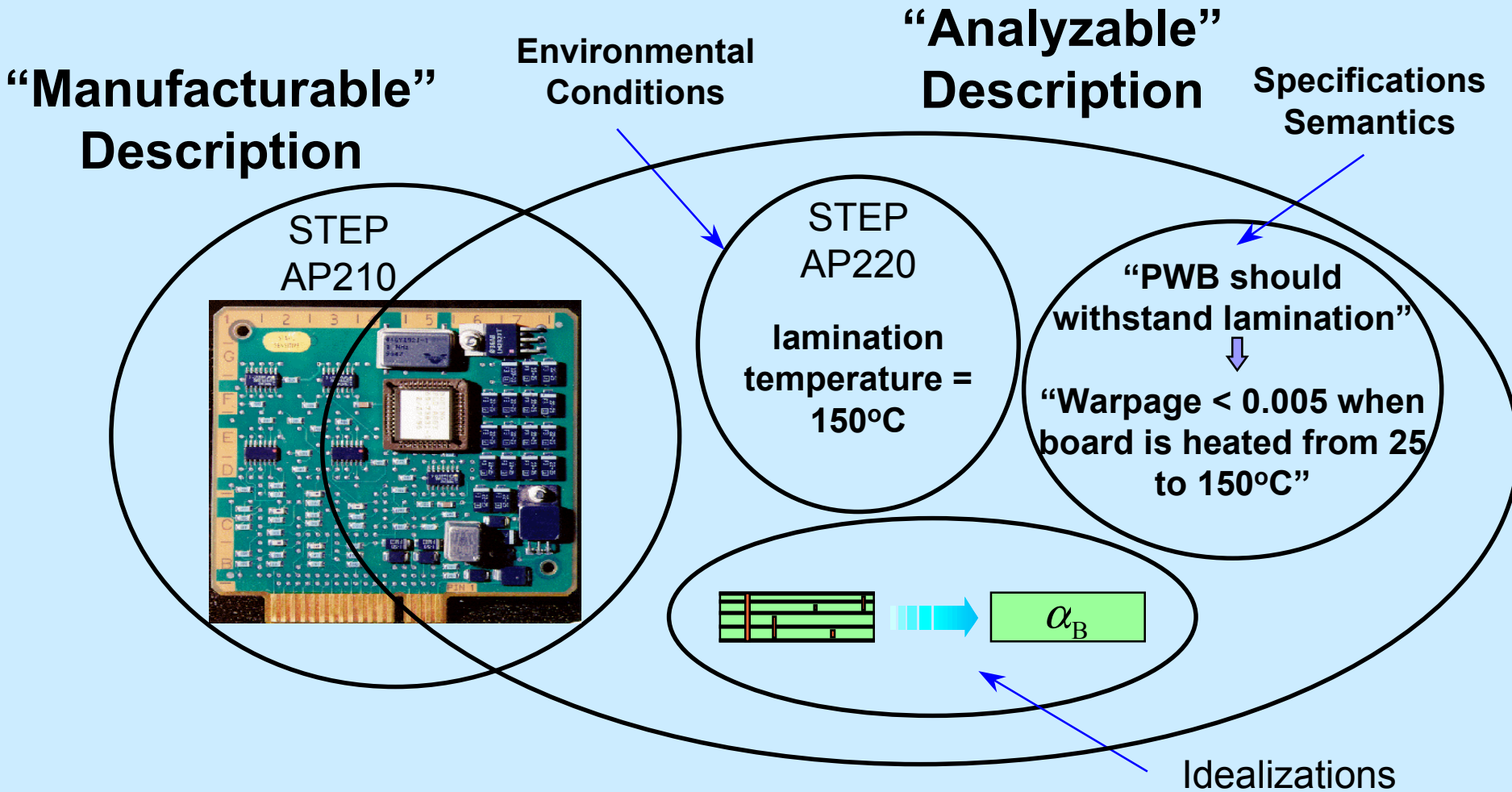
Material Properties & Geometry 1		TENSION FITTING TYPE	
Ftu = 67000 PSI	Pu = 5960 LBS	E = 10000000 PSI	<p>CHANNEL FITTING section A-A</p>
FtuT = 65000 PSI	co = 0.5240 IN	ro = 0.4375 IN	
Fty = 67000 PSI	r1 = 0.0000 IN	r2 = 0.0000 IN	
FtyLT = 52000 PSI	jm = 1.00	te = 0.500 IN	
Fsu = 39000 PSI	tw = 0.310 IN	tb = 0.307 IN	
epuT = 0.067 IN/IN	e = 1.267 IN	a = 1.770 IN	
epuLT = 0.030 IN/IN	b = 2.440 IN	h = 2.088 IN	
ftw = 3228 PSI	eta = 1.000	CU = 1.248 IN	
Agross = 1.846 IN ²	Rtw = 0.048 (Actual)	CL = 0.676 IN	
		c = 1.248 IN	
Wall Tension Analysis: Anet = 1.846 IN ² Agross = 1.846 IN ²		Wall Bending Analysis: I = 0.649 IN ⁴ mu = 3525 LB-IN	
Wall Bending & Tension Interaction: n = 1.25 gamma = 0.915		***** PLASTIC BENDING ANALYSIS ***** Rtwu = 0.490 (Allowable) Rbwu = 0.591 (Allowable) MSwall = 9.17	
End Pad Bending Analysis: K3 = 0.591 Kend = 1.500		***** PLASTIC BENDING ANALYSIS ***** fbe = 15038 PSI Fbe = 91844 PSI MSepp = 5.11	
End Pad Shear Analysis:		fse = 3620 PSI MSepp = 9.77	
Allowable Load: Pallow = 36395 LBS		WARNING: Edge distance 'h - e - tb/2' should be at least twice the hole DIAMETER (2(2ri)) from the free edge to prevent tension failure in wall.	




Fastener is LE7K18 and represented as beam element number 362 in FEA model. Load considered is 2G7T12U intact (Detent 0, Fairing Condition 1) and is obtained from the FEA model axial beam loads.

ENGR.	NAME	12/20/96	REVISED	DATE	Outboard TE Flap, Support No. 2 Bulkhead Attachment Location to 123L4567 ibbulk.tem ibbulk.dta ENGINEER DEVELOPED TEMPLATE	129-300
CHECK						
APR						
APR						
FCM	s734c07-PROD	IAS				PAGE 206

Analysis Integration Challenges: Information Diversity



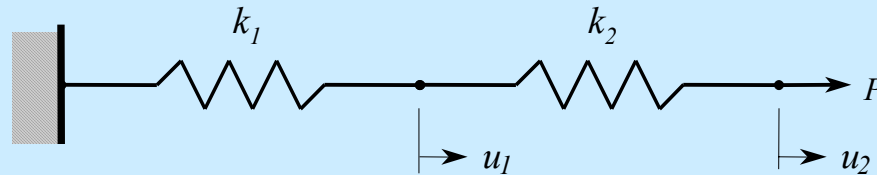
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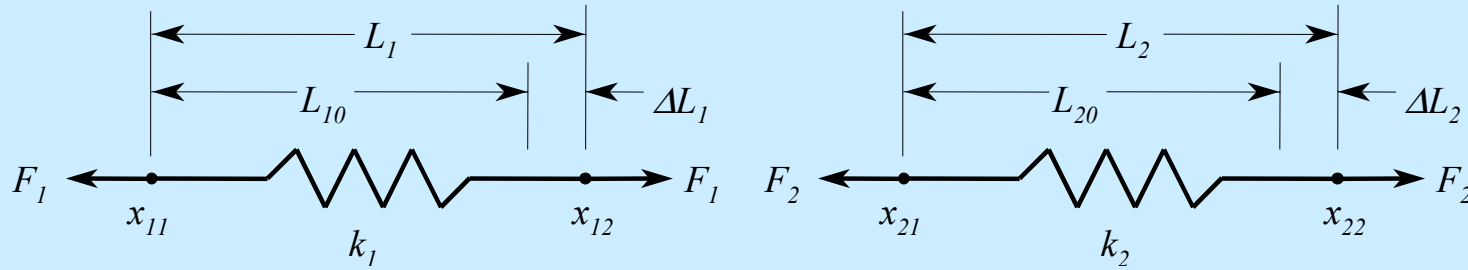
Traditional Mathematical Representation

Two Spring System

System Figure



Free Body Diagrams



Variables and Relations

Kinematic Relations

$$r_{11} : L_1 = x_{12} - x_{11}$$

$$r_{12} : \Delta L_1 = L_1 - L_{10}$$

$$r_{13} : F_1 = k_1 \Delta L_1$$

$$r_{21} : L_2 = x_{22} - x_{21}$$

$$r_{22} : \Delta L_2 = L_2 - L_{20}$$

$$r_{23} : F_2 = k_2 \Delta L_2$$

$$bc_1 : x_{11} = 0$$

$$bc_2 : x_{12} = x_{21}$$

$$bc_3 : F_1 = F_2$$

$$bc_4 : F_2 = P$$

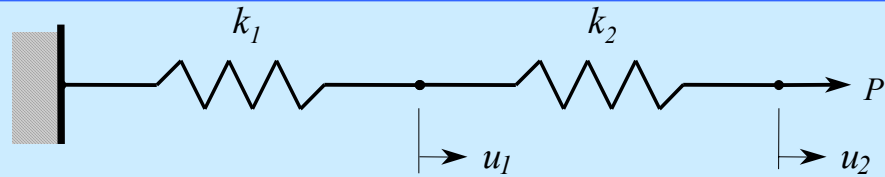
$$bc_5 : u_1 = \Delta L_1$$

$$bc_6 : u_2 = \Delta L_2 + u_1$$

Boundary Conditions

Constraint Graph

Two Spring System



$$r_{11} : L_1 = x_{12} - x_{11}$$

$$r_{12} : \Delta L_1 = L_1 - L_{10}$$

$$r_{13} : F_1 = k_1 \Delta L_1$$

$$r_{21} : L_2 = x_{22} - x_{21}$$

$$r_{22} : \Delta L_2 = L_2 - L_{20}$$

$$r_{23} : F_2 = k_2 \Delta L_2$$

$$bc_1 : x_{11} = 0$$

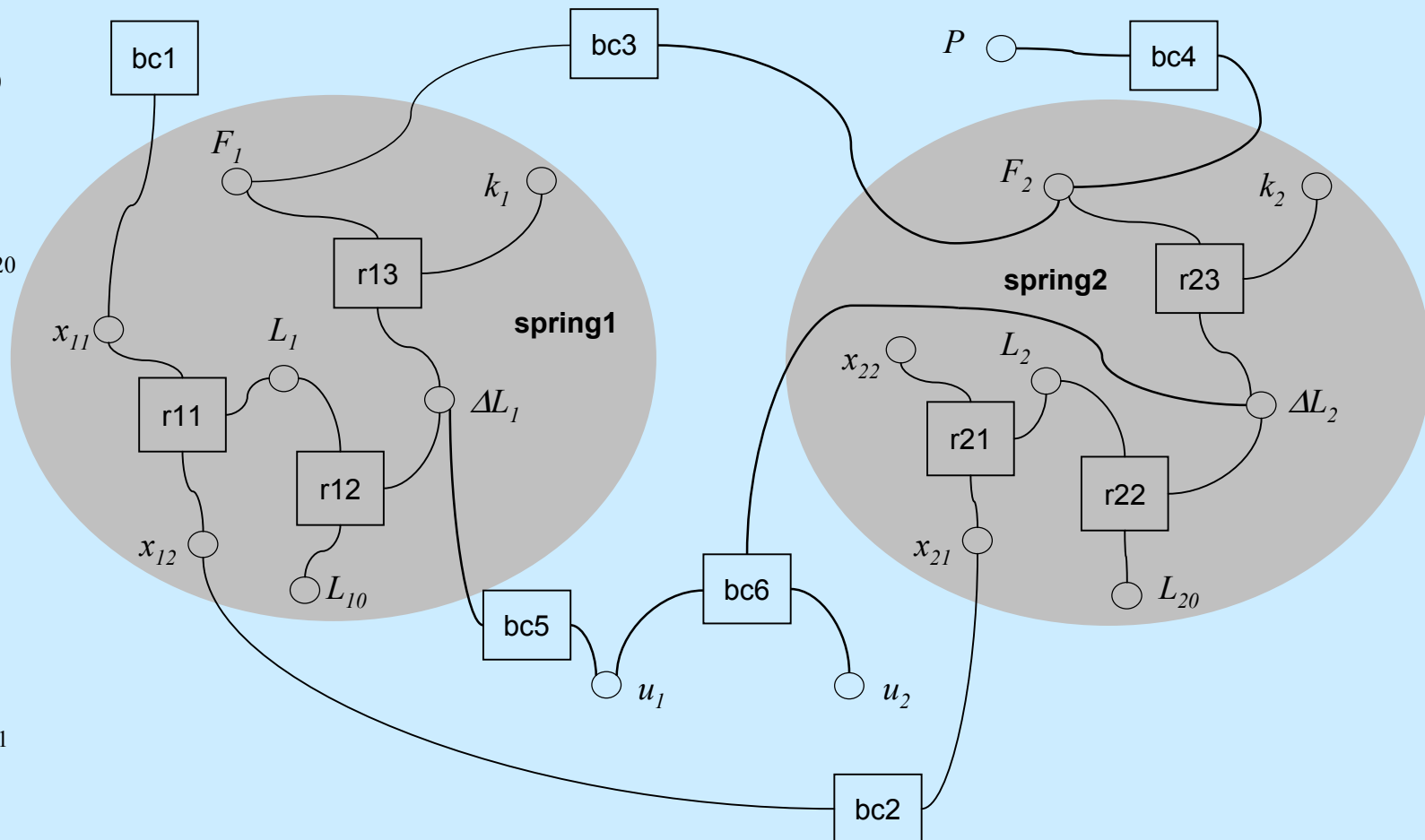
$$bc_2 : x_{12} = x_{21}$$

$$bc_3 : F_1 = F_2$$

$$bc_4 : F_2 = P$$

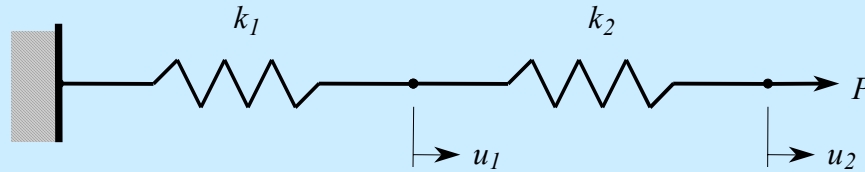
$$bc_5 : u_1 = \Delta L_1$$

$$bc_6 : u_2 = \Delta L_2 + u_1$$



COB Constraint Schematic

Two Spring System



*Analysis Primitives
with
Encapsulated Relations*

$$r_{11} : L_1 = x_{12} - x_{11}$$

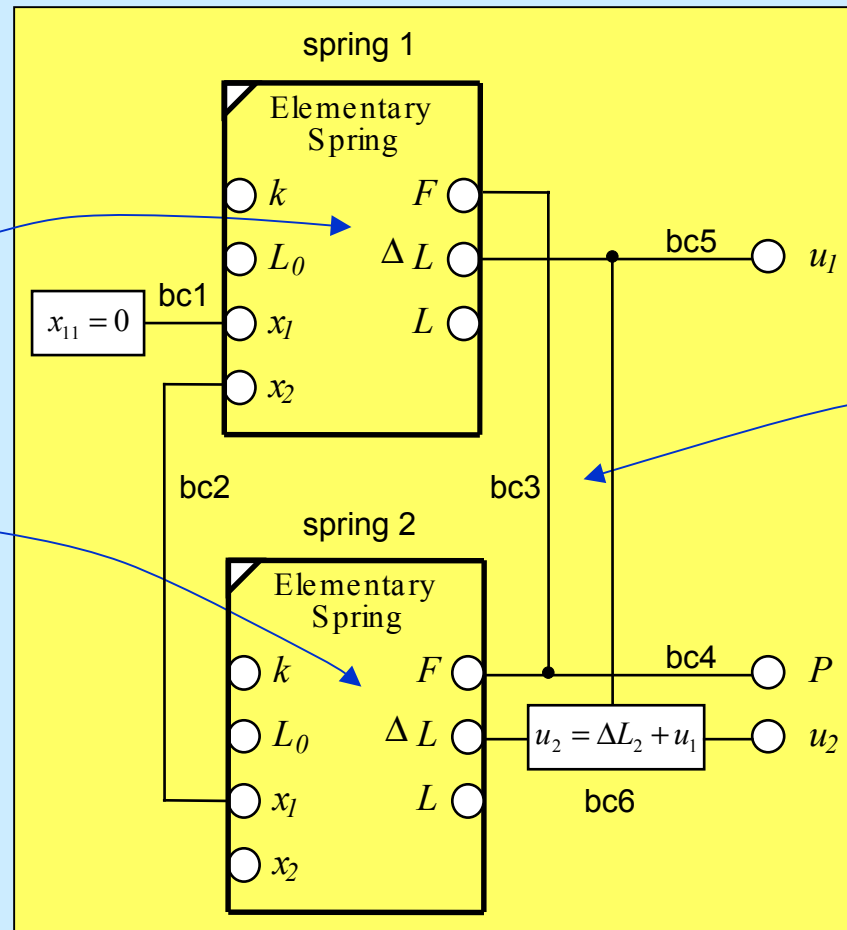
$$r_{12} : \Delta L_1 = L_1 - L_{10}$$

$$r_{13} : F_1 = k_1 \Delta L_1$$

$$r_{21} : L_2 = x_{22} - x_{21}$$

$$r_{22} : \Delta L_2 = L_2 - L_{20}$$

$$r_{23} : F_2 = k_2 \Delta L_2$$



*System-Level Relations
(Boundary Conditions)*

$$bc_1 : x_{11} = 0$$

$$bc_2 : x_{12} = x_{21}$$

$$bc_3 : F_1 = F_2$$

$$bc_4 : F_2 = P$$

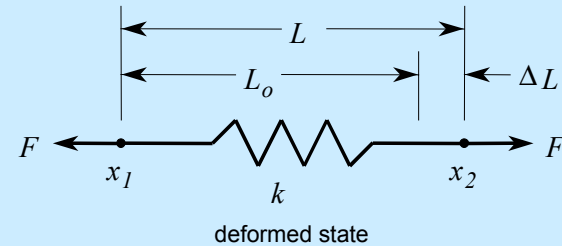
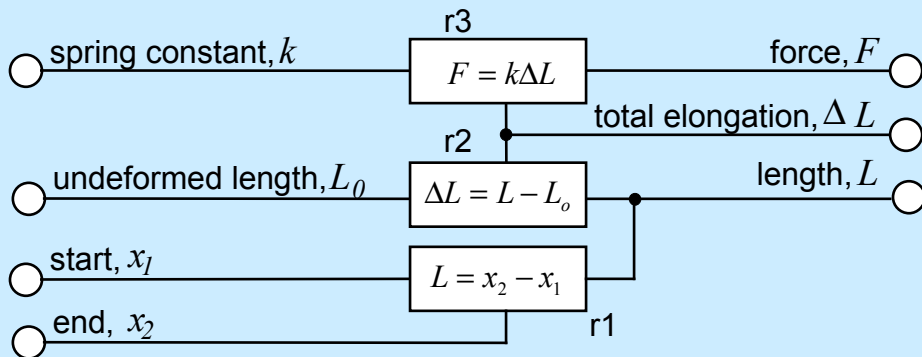
$$bc_5 : u_1 = \Delta L_1$$

$$bc_6 : u_2 = \Delta L_2 + u_1$$

COB Structure: Graphical Forms

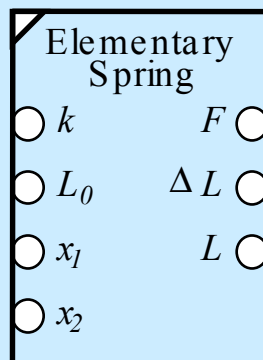
Spring Primitive

Constraint Schematic



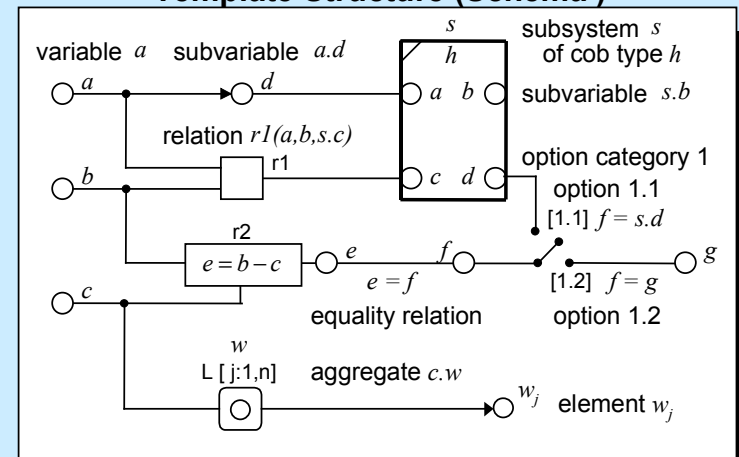
Subsystem View

(for reuse by other COBs)



Basic Constraint Schematic Notation

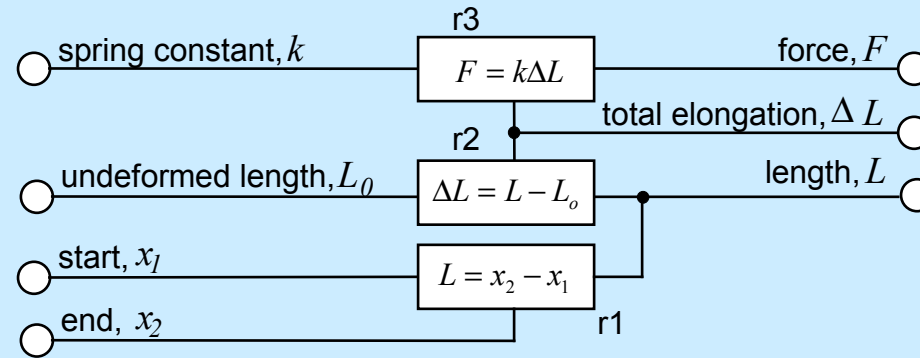
Template Structure (Schema)



COB Structure: Lexical Form

Spring Primitive

Constraint Schematic

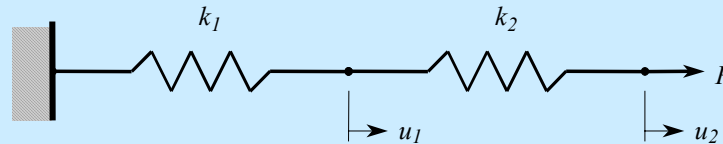


Lexical COB Schema Template

```
COB spring SUBTYPE_OF abb;
  undeformed_length, L<sub>0</sub> : REAL;
  spring_constant, k : REAL;
  start, x<sub>1</sub> : REAL;
  end, x<sub>2</sub> : REAL;
  length, L : REAL;
  total_elongation, &Delta;L : REAL;
  force, F : REAL;
RELATIONS
  r1 : "<length> == <end> - <start>";
  r2 : "<total_elongation> == <length> - <undeformed_length>";
  r3 : "<force> == <spring_constant> * <total_elongation>";
END_COB;
```

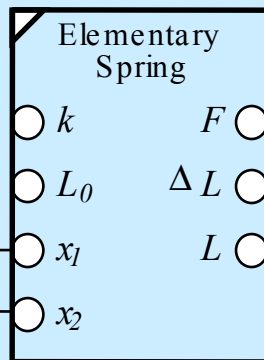
COBs as Building Blocks

Two Spring System

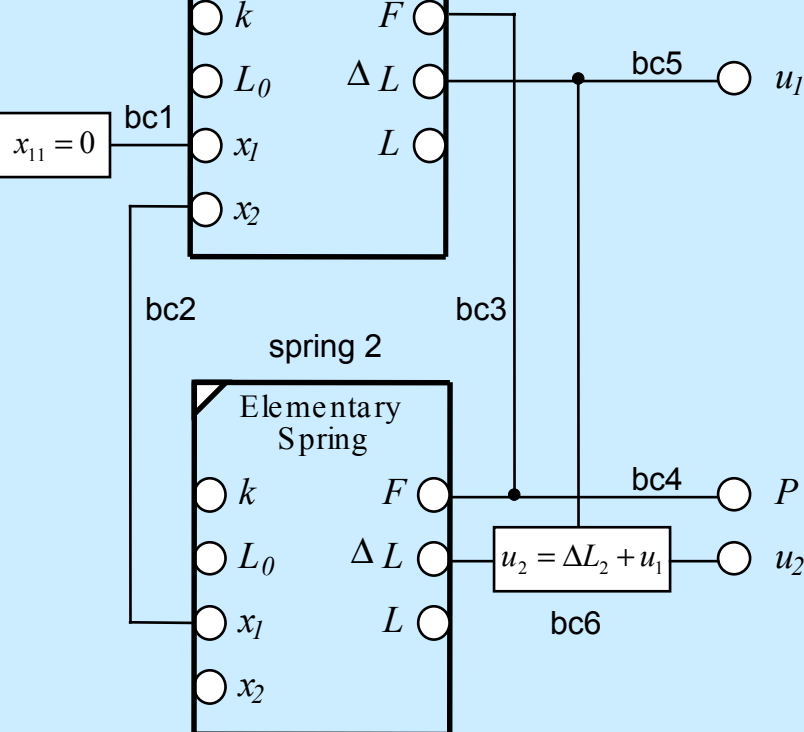
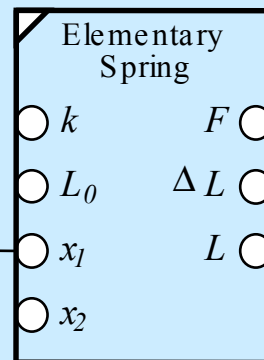


Constraint Schematic

spring 1



spring 2



Lexical COB Schema Template

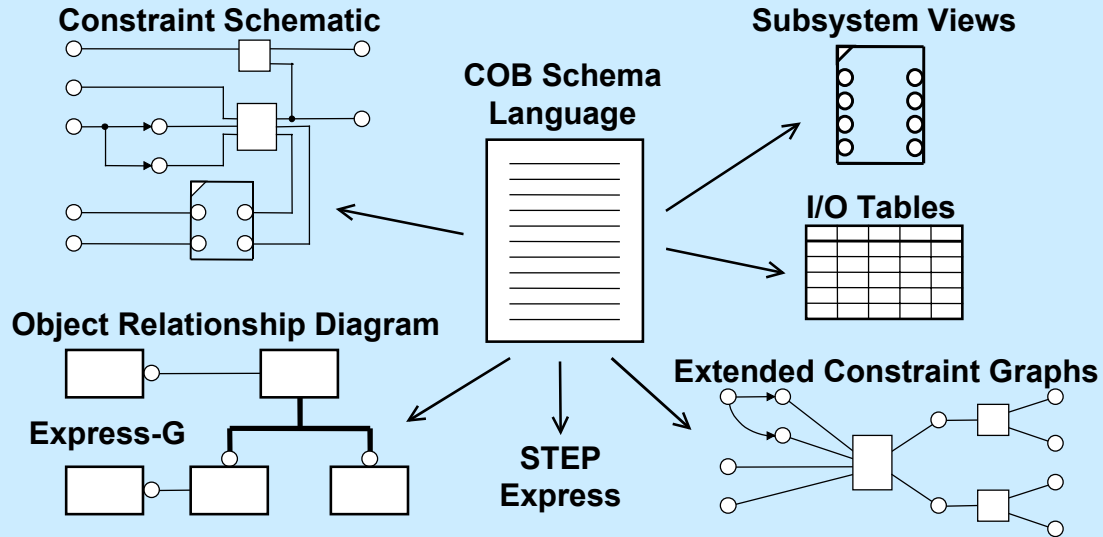
```

COB spring_system SUBTYPE_OF analysis_system;
spring1 : spring;
spring2 : spring;
deformation1, u<sub>1</sub> : REAL;
deformation2, u<sub>2</sub> : REAL;
load, P : REAL;

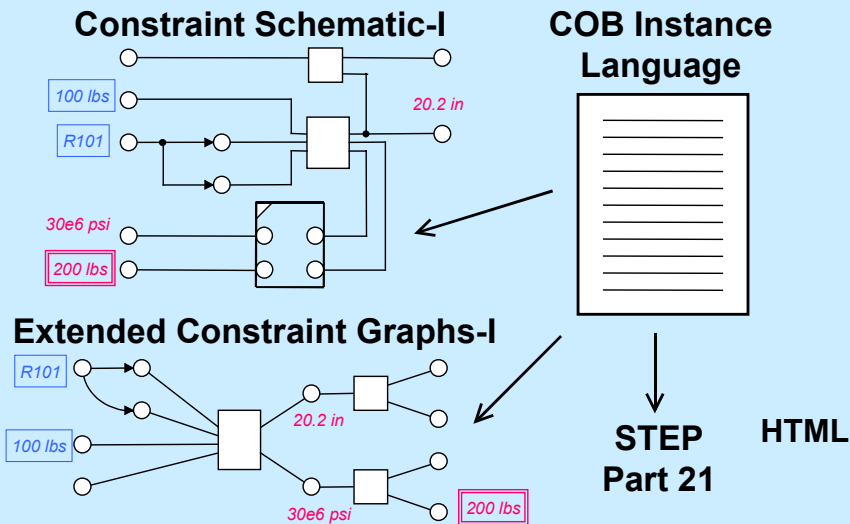
RELATIONS
bc1 : "<spring1.start> == 0.0";
bc2 : "<spring1.end> == <spring2.start>";
bc3 : "<spring1.force> == <spring2.force>";
bc4 : "<spring2.force> == <load>";
bc5 : "<deformation1> == <spring1.total_elongation>";
bc6 : "<deformation2> == <spring2.total_elongation>
      + <deformation1>";

END_COB;
    
```

COB Modeling Views



HTML

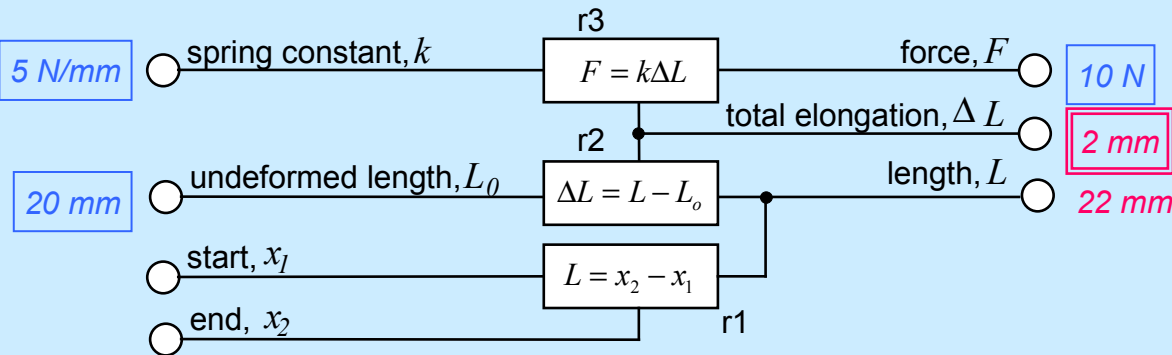


Example COB Instance

Spring Primitive

Constraint Schematic Instance Views

example 1, state 1



Lexical COB Instances

input:

```

INSTANCE_OF spring;
    undeformed_length : 20.0;
    spring_constant : 5.0;
    start : ?;
    end : ?;
    length : ?;
    total_elongation : ?;
    force : 10.0;
END_INSTANCE;

```

result (reconciled):

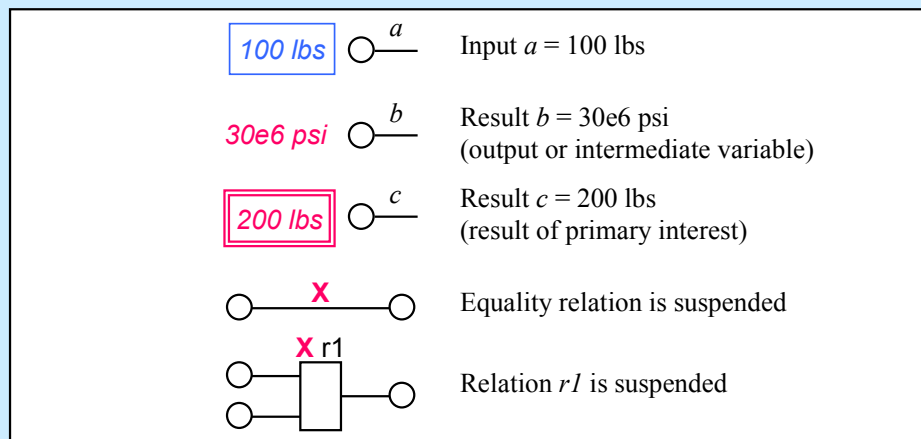
```

INSTANCE_OF spring;
    undeformed_length : 20.0;
    spring_constant : 5.0;
    start : ?;
    end : ?;
    length : 22.0;
    total_elongation : 2.0;
    force : 10.0;
END_INSTANCE;

```

Basic Constraint Schematic Notation

Instances

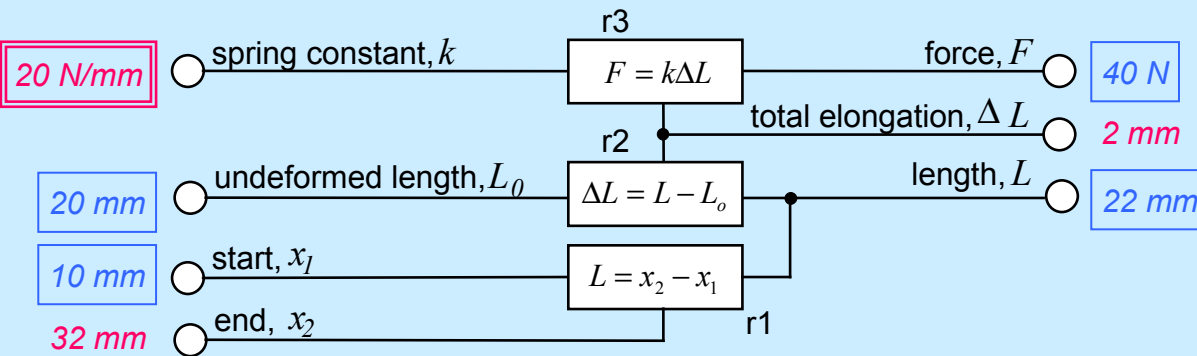


Multidirectional I/O

Spring Primitive

Constraint Schematic Instance View

example 1, state 5



Lexical COB Instance

input:

```

INSTANCE_OF spring;
  undeformed_length : 20.0;
  spring_constant : ?;
  start : 10.0;
  end : ?;
  length : 22.0;
  total_elongation : ?;
  force : 40.0;
END_INSTANCE;

```

result:

```

INSTANCE_OF spring;
  undeformed_length : 20.0;
  spring_constant : 20.0;
  start : 10.0;
  end : 32.0;
  length : 22.0;
  total_elongation : 2.0;
  force : 40.0;
END_INSTANCE;

```

Spring Examples Implemented in *XaiTools* X-Analysis Integration Toolkit

spring

Name	Symbol	Type	Input	Values
root		spring		
undeformed_length	$L_{₀}$	REAL	Input	20
spring_constant	k	REAL	Input	5
start	$x_{₁}$	REAL	Output	No value
end0	$x_{₂}$	REAL	Output	No value
length	L	REAL	Output	22
total_elongation	ΔL	REAL	Output	2
force	F	REAL	Input	10

Solve

root (spring)

Name	Local	Oneway	Relation	Active
r1	Y		$\langle \text{length} \rangle == \langle \text{end0} \rangle - \langle \text{start} \rangle$	<input checked="" type="checkbox"/>
r2	Y		$\langle \text{total_elongation} \rangle == \langle \text{length} \rangle - \langle \text{undeformed_length} \rangle$	<input checked="" type="checkbox"/>
r3	Y		$\langle \text{force} \rangle == \langle \text{spring_constant} \rangle * \langle \text{total_elongation} \rangle$	<input checked="" type="checkbox"/>

spring_system

Name	Symbol	Type	Input	Values
root		spring_system		
spring1		spring		
undeformed_length	$L_{₀}$	REAL	Input	8
spring_constant	k	REAL	Input	5
start	$x_{₁}$	REAL	Output	0
end0	$x_{₂}$	REAL	Output	10
length	L	REAL	Output	10
total_elongation	ΔL	REAL	Output	2
force	F	REAL	Output	10
spring2		spring		
undeformed_length	$L_{₀}$	REAL	Input	8
spring_constant	k	REAL	Input	20
start	$x_{₁}$	REAL	Output	10
end0	$x_{₂}$	REAL	Output	18.5
length	L	REAL	Output	8.5
total_elongation	ΔL	REAL	Output	0.5
force	F	REAL	Output	10
deformation1	$u_{₁}$	REAL	Output	2
deformation2	$u_{₂}$	REAL	Output	2.5
load	P	REAL	Input	10

Solve

root (spring_system)

Name	Local	Oneway	Relation	Active
r1	Y		$\langle \text{spring1.start} \rangle == 0.0$	<input checked="" type="checkbox"/>
r2	Y		$\langle \text{spring1.end0} \rangle == \langle \text{spring2.start} \rangle$	<input checked="" type="checkbox"/>
r3	Y		$\langle \text{spring1.force} \rangle == \langle \text{spring2.force} \rangle$	<input checked="" type="checkbox"/>
r4	Y		$\langle \text{spring2.force} \rangle == \langle \text{load} \rangle$	<input checked="" type="checkbox"/>
r5	Y		$\langle \text{deformation1} \rangle == \langle \text{spring1.total_elongation} \rangle$	<input checked="" type="checkbox"/>
r6	Y		$\langle \text{deformation2} \rangle == \langle \text{spring2.total_elongation} \rangle + \langle \text{deformation1} \rangle$	<input checked="" type="checkbox"/>

spring

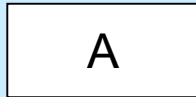
Name	Symbol	Type	Input	Values
root		spring		
undeformed_length	$L_{₀}$	REAL	Input	20
spring_constant	k	REAL	Output	20
start	$x_{₁}$	REAL	Input	10
end0	$x_{₂}$	REAL	Output	32
length	L	REAL	Input	22
total_elongation	ΔL	REAL	Output	2
force	F	REAL	Input	40

Solve

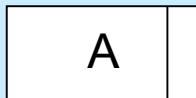
root (spring)

Name	Local	Oneway	Relation	Active
r1	Y		$\langle \text{length} \rangle == \langle \text{end0} \rangle - \langle \text{start} \rangle$	<input checked="" type="checkbox"/>
r2	Y		$\langle \text{total_elongation} \rangle == \langle \text{length} \rangle - \langle \text{undeformed_length} \rangle$	<input checked="" type="checkbox"/>
r3	Y		$\langle \text{force} \rangle == \langle \text{spring_constant} \rangle * \langle \text{total_elongation} \rangle$	<input checked="" type="checkbox"/>

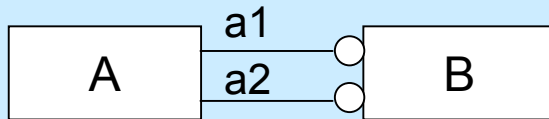
Basic EXPRESS-G notation



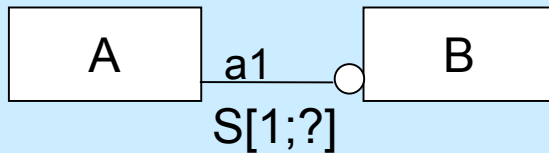
A is an entity (class)
Instance of A are objects



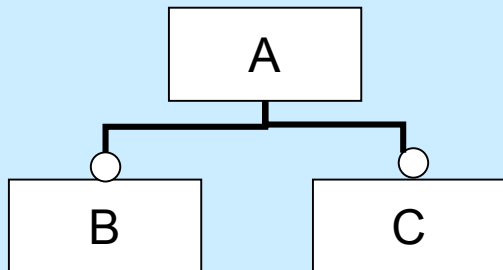
A is a simple type
(BOOLEAN, LOGICAL, BINARY,
NUMBER, INTEGER, REAL, STRING)



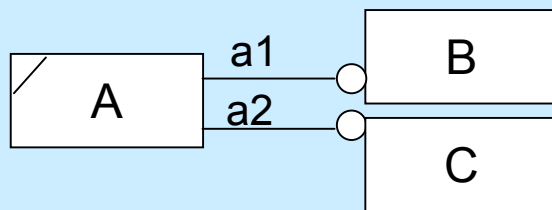
A has two attribute, a1 and a2, that
are both type B



A has an attribute, a1, that is
a Set of 1 or ore entities of type B

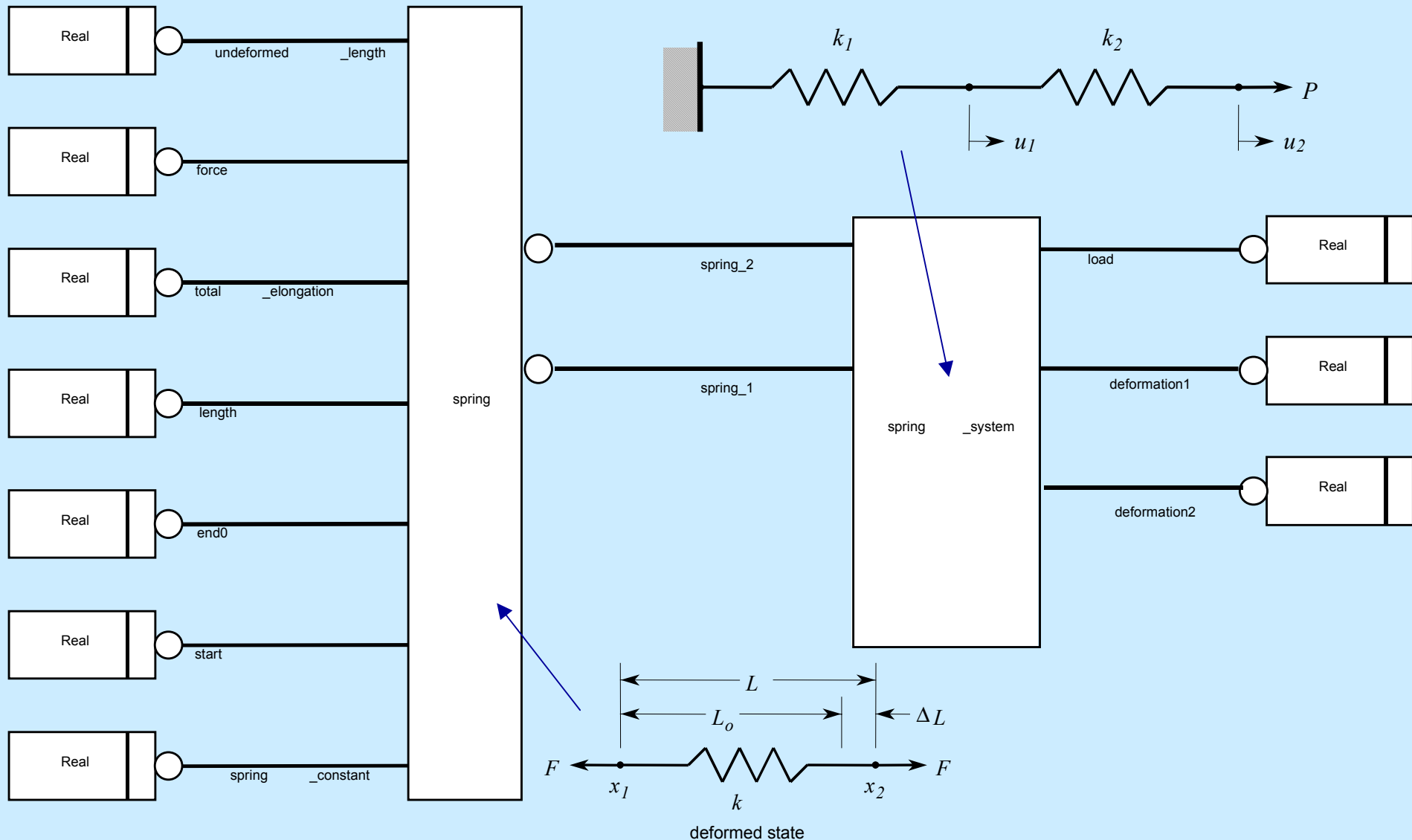


A is a supertype of B and C.
(B and C are subtype of A)



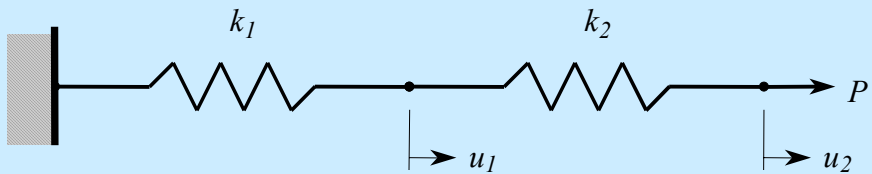
Unofficial extensions:
A has two levels, a1 and a2.
a1 is type B. a2 is type C.

COB Object Model View (EXPRESS-G) Spring Schema



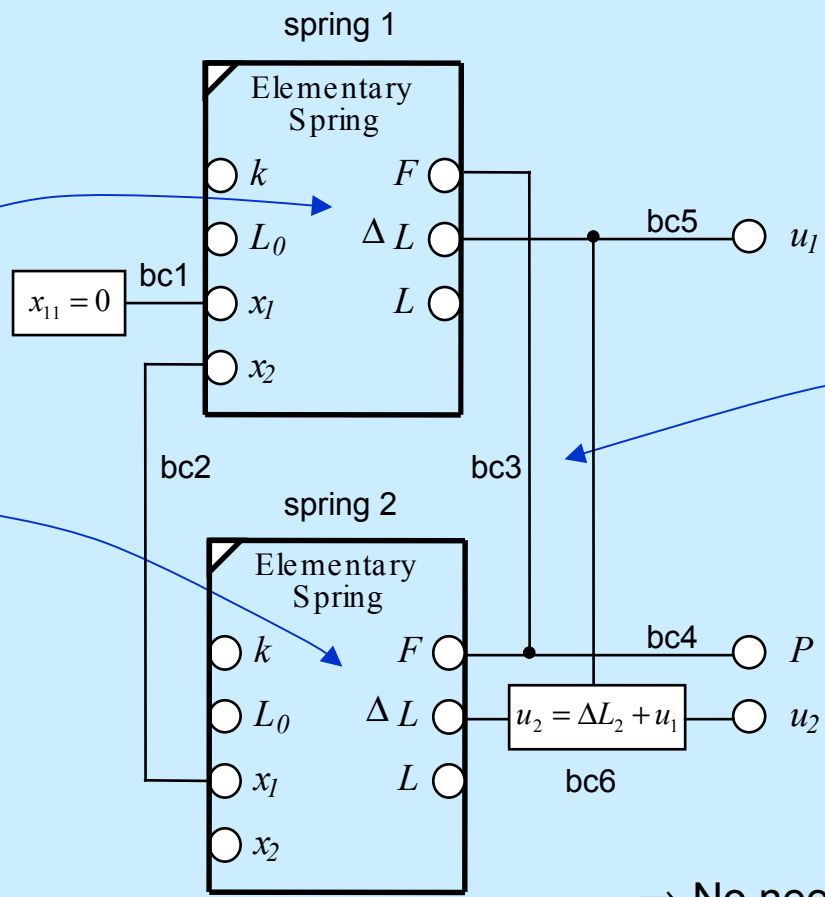
Declarative Knowledge / Derivable Behavior

Two Spring System



$r_{11} : L_1 = x_{12} - x_{11}$
 $r_{12} : \Delta L_1 = L_1 - L_{10}$
 $r_{13} : F_1 = k_1 \Delta L_1$

$r_{21} : L_2 = x_{22} - x_{21}$
 $r_{22} : \Delta L_2 = L_2 - L_{20}$
 $r_{23} : F_2 = k_2 \Delta L_2$



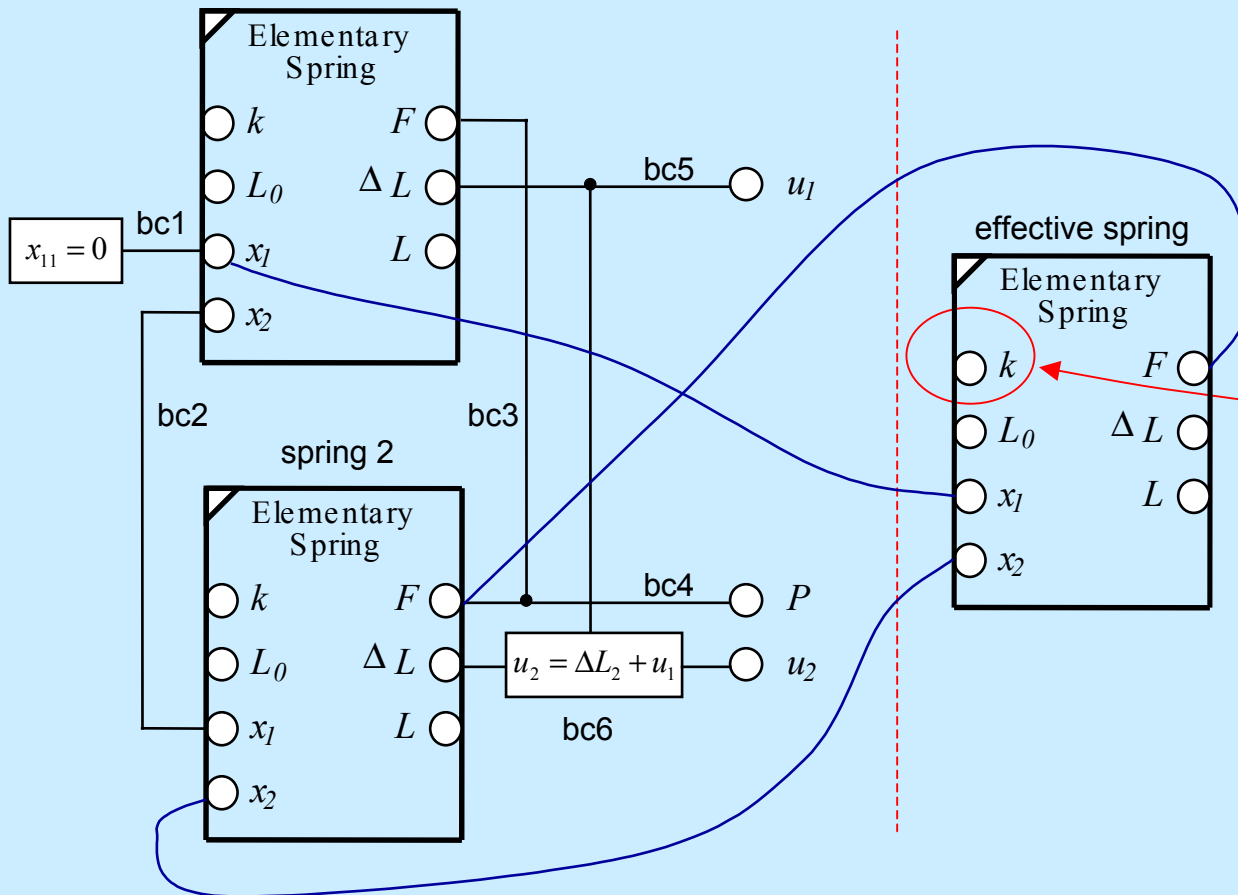
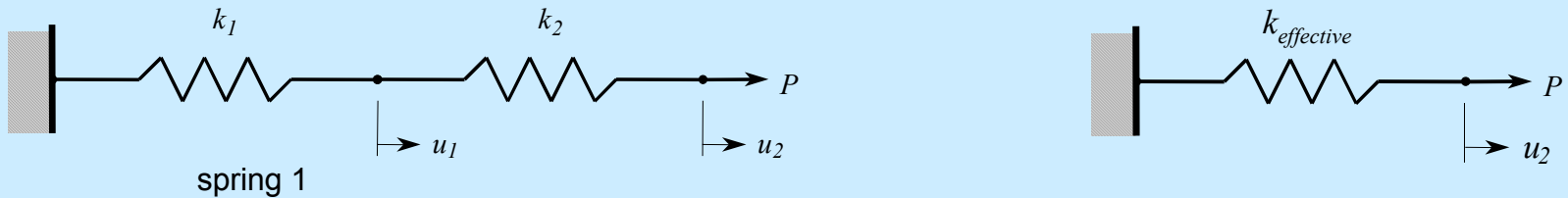
$bc_1 : x_{11} = 0$
 $bc_2 : x_{12} = x_{21}$
 $bc_3 : F_1 = F_2$
 $bc_4 : F_2 = P$
 $bc_5 : u_1 = \Delta L_1$
 $bc_6 : u_2 = \Delta L_2 + u_1$

Derivable Behavior

$dr_1 : u_1 = \frac{P}{k_1}$
 $dr_2 : u_2 = P \frac{k_1 + k_2}{k_1 k_2}$

⇒ No need to include explicitly (redundant)

Achieving Effective System Properties via Semantically Rich COBs



Derivable System Level Properties

$$dr_1: k_{effective} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}}$$

$$dr_2: \Delta L_{effective} = \Delta L_1 + \Delta L_2$$

etc.

- ⇒ No need to derive
- ⇒ Minimal extra work
- ⇒ Semantically richer

Constrained Object Language (COBs)

◆ Capabilities & features

- Various forms: computable lexical form, graphical form, etc.
- Sub/supertypes, basic aggregates, multifidelity objects
- Multidirectionality (I/O change)
- Wrapping external programs as black box relations

◆ Analysis module/template applications:


- Product model idealizations
- Explicit associativity relations with design models & other analyses
- Black box reuse of existing tools (e.g., FEA tools, in-house functions)
- Reusable, adaptable analysis building blocks
- Synthesis (sizing) and verification (analysis)

Constrained Object Language (cont.)

◆ Summary

- Declarative knowledge representation combining objects & constraints
- COBs = (STEP EXPRESS subset) + (constraint concepts & views)
- Advantages over traditional representations:
 - » Greater solution control
 - » Richer semantics (e.g., equations wrapped in engineering context)
 - » Capture of reusable knowledge

Outline

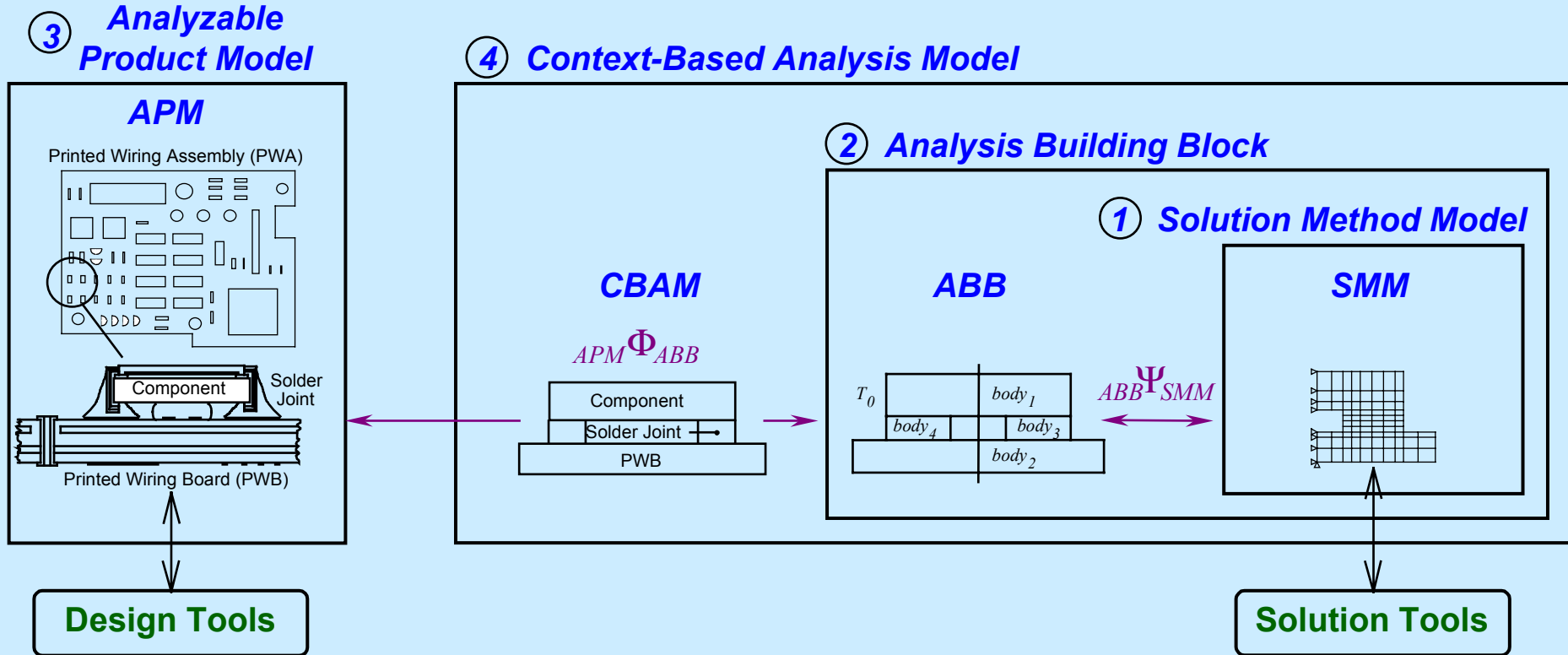
- ◆ Analysis Integration Challenges
- ◆ Introduction to Constrained Objects (COBs)
- ◆ Overview of COB-based XAI 
- ◆ Example Applications
 - ◆ Electronic Packaging Thermomechanical Analysis
 - ◆ Aerospace Structural Analysis
- ◆ Summary

Components of the MRA Analysis Integration Technique

- ◆ Conceptual architecture: MRA
- ◆ Methodology
- ◆ General purpose MRA toolkit: *XaiTools*
 - Toolkit architecture
 - Users guide
 - Tutorials (work-in-process)
- ◆ Product/company-specific applications
 - PWA/Bs (ProAM)
 - Aerospace structural analysis (Boeing PSI)
 - Chip packaging/mounting (Shinko)

See <http://eislabs.gatech.edu/> for references

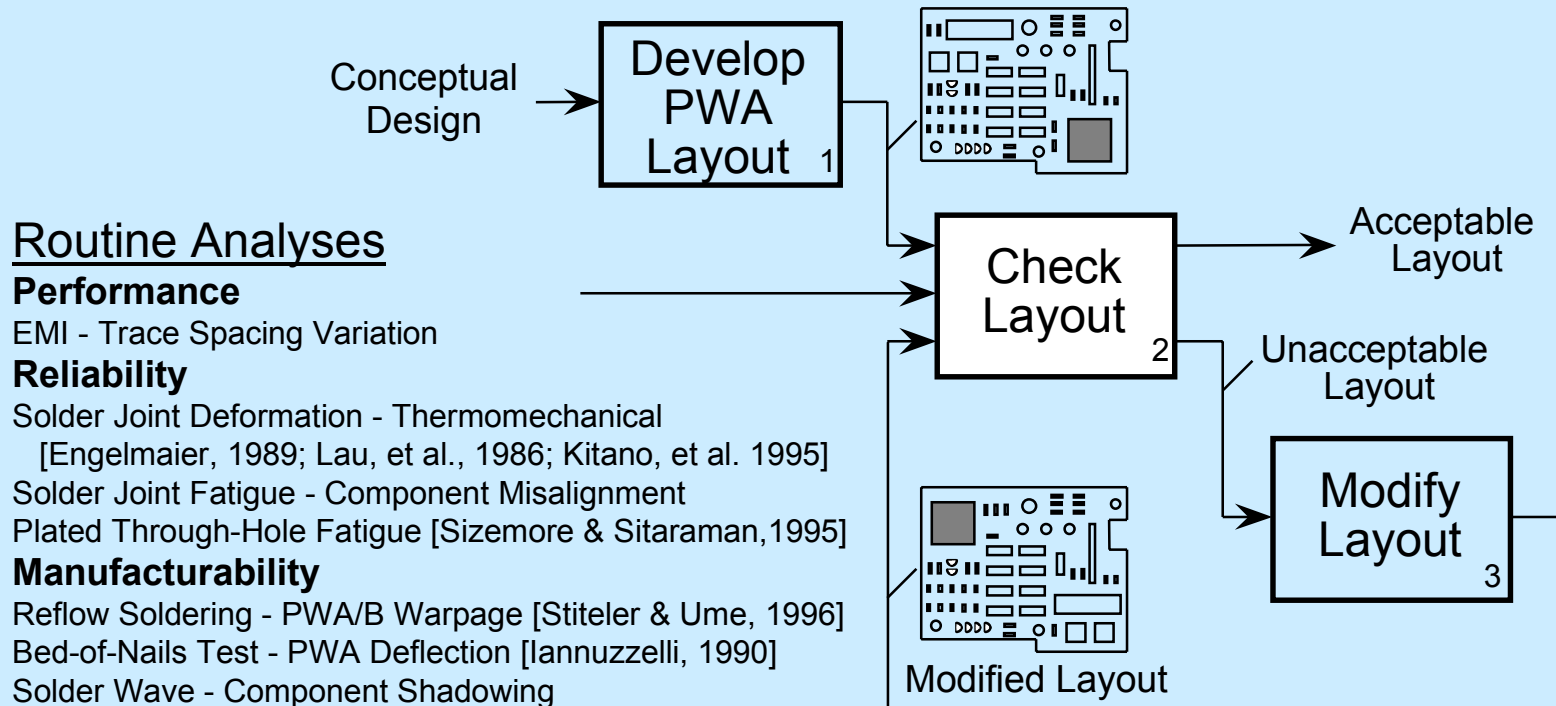
Multi-Representation Architecture for Design-Analysis Integration



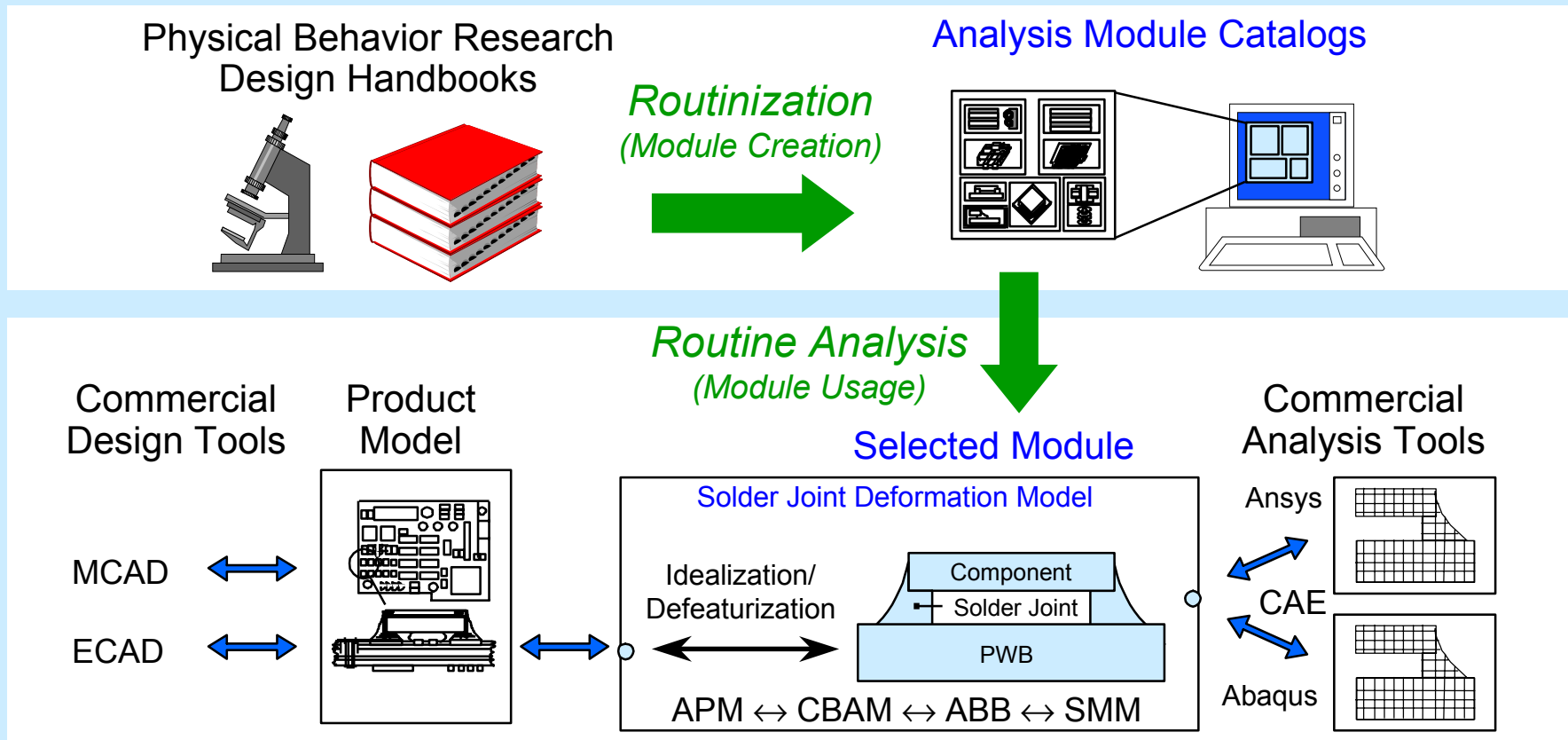
- ◆ Composed of four representations (information models)
- ◆ Provides flexible, modular mapping between design & analysis models
- ◆ Creates automated, product-specific analysis modules (CBAMs)
- ◆ Represents design-analysis associativity explicitly

Routine Analysis: Opportunity for Automation

Typical PWA Design Process



Design-Analysis Integration Methodology

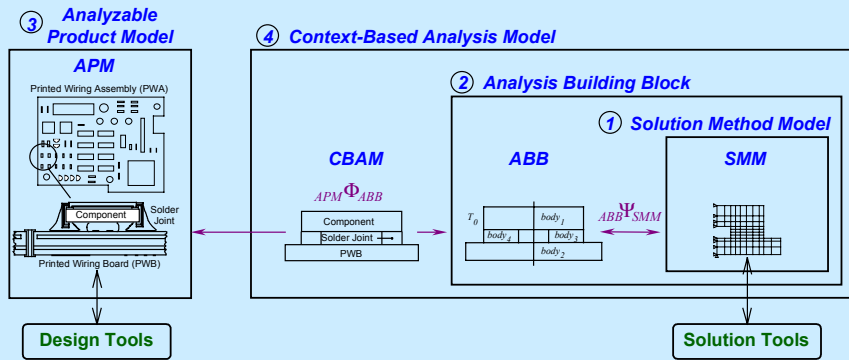


- ◆ Provides technique to bridge CAD-CAE gap
- ◆ Uses AI & info. technology: objects, constraints, STEP

XaiTools

Prototype X-Analysis Integration Toolkit Second Generation - Java-based

Multi-Representation Architecture (MRA)

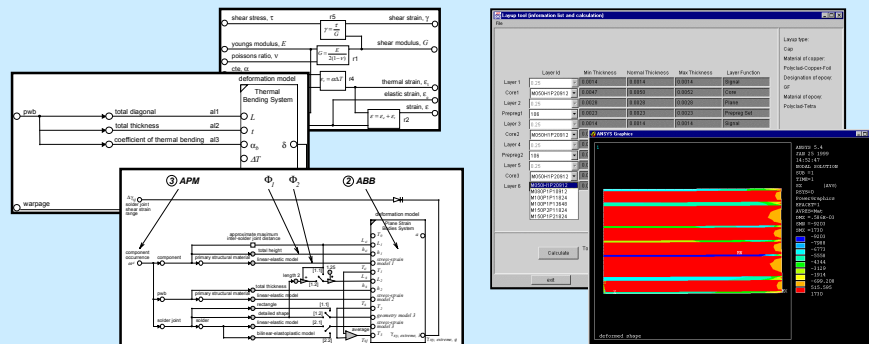


- ◆ Product-independent MRA toolkit
- ◆ Lexical constrained objects (COBs)
 - Data-driven creation
 - User-adaptable
- ◆ Mathematica constraint solver
 - More capabilities
- ◆ SMM-type wrappings:
 - FEA tools: Ansys, Abaqus*
 - Symbolic Eqn. Solver: Mathematica
- ◆ Extended APM technique for design links:
 - CATIA MCAD modeler
- ◆ Updates/Extensions in progress*:
 - PWB/A: GenCAM; STEP AP210-based APM link w/ Mentor Graphics BoardStation
 - Generalized MCAD modeler links
 - Advanced parametric FEA transformation
 - Object-Oriented Optimization
 - CORBA-based tool interchanges
 - XML views of analysis results etc.

Analysis Modules & Building Blocks

Constraint Schematics

Implementations



XaiTools Tool Architecture

Company/Product-Independent View

Capabilities as of 12/98

Plus ECAD AP210 link
and items from first gen. prototypes:
full SMMs, complex meshing, etc.

Design Tools

MCAD Tool

CATIA

Material Properties Manager

MATDB-like files

Standard Parts Manager

FASTDB-like files

Tagging Technique &
Interpretive
CATGEO
Interface

COB Instances

objects, x.coi, x.step

Tool Forms
(parameterized tool
models/partial SMMs)

Template Libraries: *CBAMs, ABBs, APMs*
Instances: *Usage/adaptation of templates*

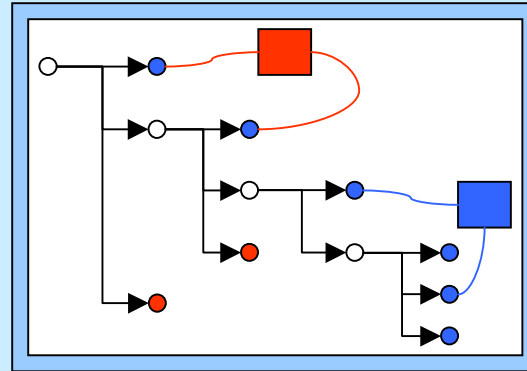
COB Schemas

objects, x.cos, x.exp

Examples:

*aerospace, electronics,
tutorials*

COB Server XaiTools



Analysis Codes

FEA: *Ansys*
General Math: *Mathematica*

Constraint Solver

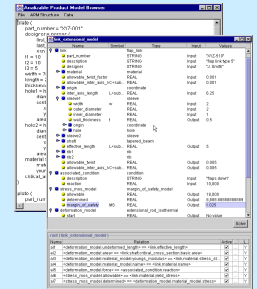
Mathematica

CORBA Wrapper

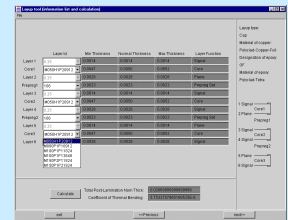
Analysis Mgt. Tools

COB Analysis Tools

Navigator: *XaiTools*
Editor (text): *WordPad*



Custom Tools



XaiTools Tool Architecture

Company/Product-Independent View
 In-Progress & Potential Extensions as of 6/99

Design Tools

MCAD: CATIA

IDEAS*, Pro/E*, AutoCAD*

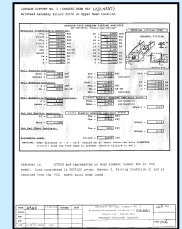
ECAD: Mentor Graphics (AP210)

Accel (PDF, GenCAM)*

Template Libraries: Analysis Packages*, CBAMs, ABBs, APMs, Conditions*
Instances: Usage/adaptation of templates

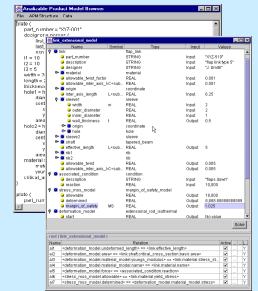
Analysis Mgt. Tools

Pullable Views*, Condition Mgr*, ...

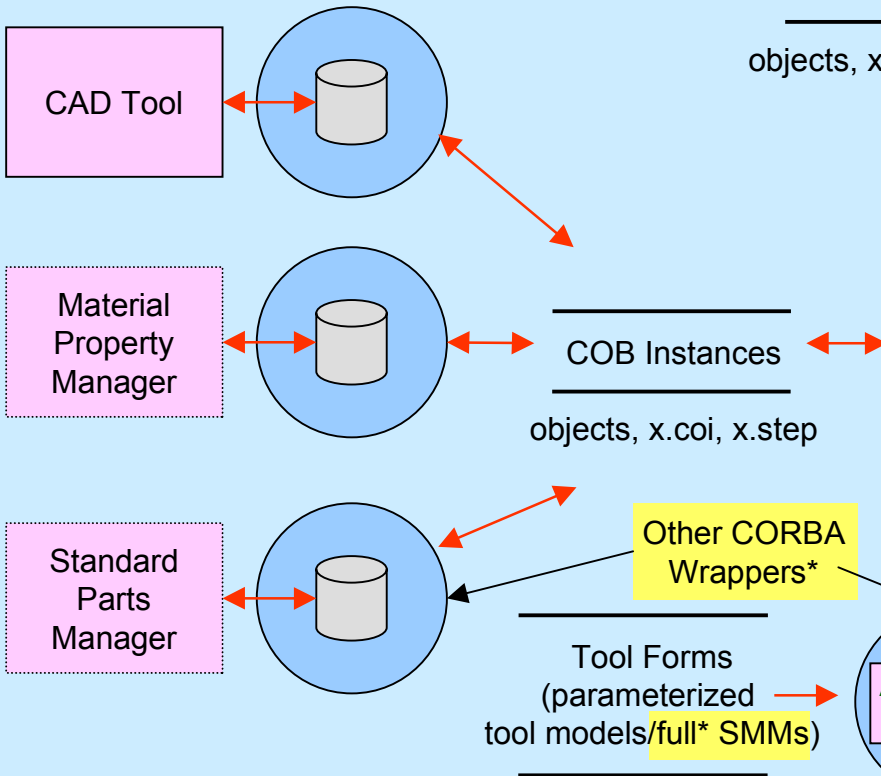
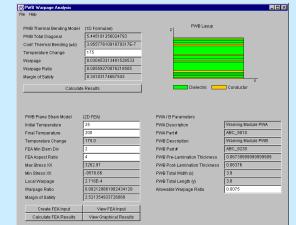


COB Analysis Tools

Navigator: XaiTools Editor (text & graphical*)



Custom Tools

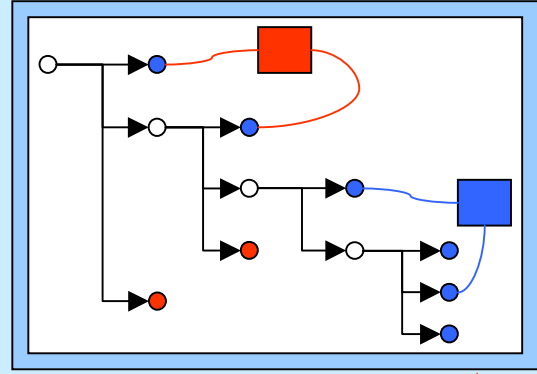


COB Schemas

objects, x.cos, x.exp

Persistent Object Repository
 ODBMS*, PDM*

COB Server



COB Instances

objects, x.coi, x.step

Other CORBA Wrappers*

Tool Forms (parameterized tool models/full* SMMs)

Analysis Codes

Constraint Solver

FEA: Ansys, Elfini*, Abaqus*

Math: Mathematica, MatLab*, MathCAD*

In-House Codes

Mathematica

CORBA Wrapper

asterisk (*) = in-progress/envisoned extensions

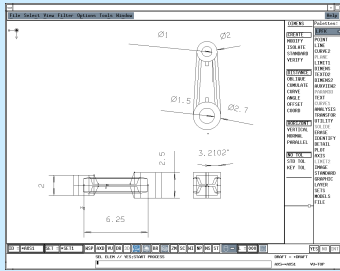
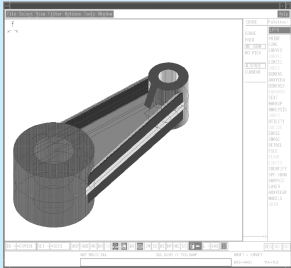
Flexible High Diversity Design-Analysis Integration

Tutorial Examples: Flap Link (Mechanical/Structural Analysis)

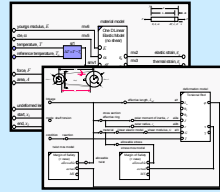
Design Tools

MCAD Tools

CATIA



Materials DB



Modular, Reusable Template Libraries

Analyzable Product Model

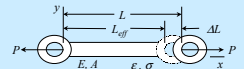


Analysis Modules (CBAMs) of Diverse Mode & Fidelity

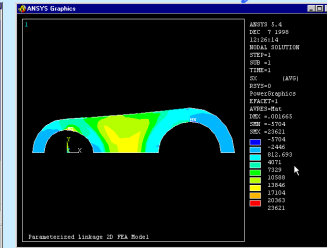
XaiTools

Analysis Tools

General Math Mathematica



FEA Ansys



Extension

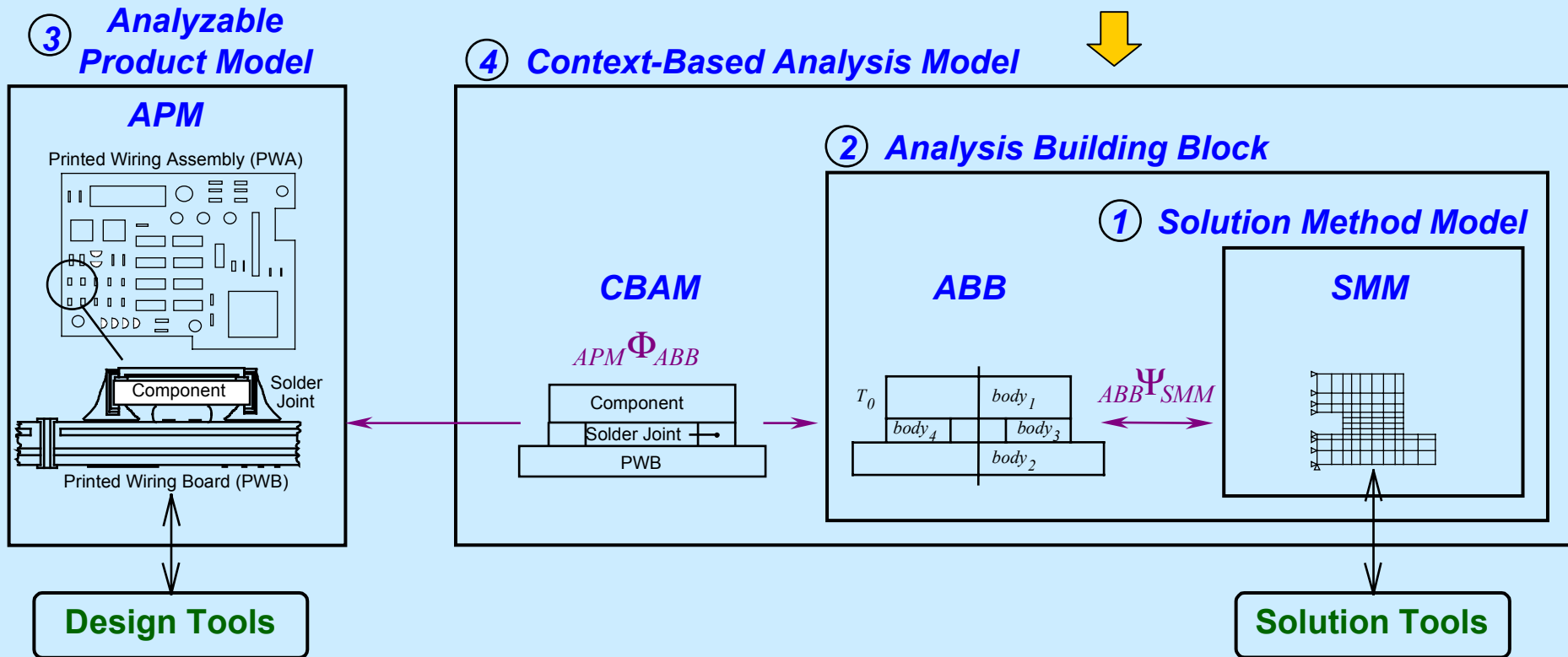
1D,
2D,
3D*

Torsion

1D

* = Item not yet available in toolkit (all others have working examples)

Multi-Representation Architecture for Design-Analysis Integration



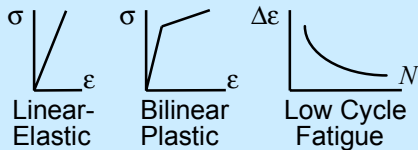
Analysis Building Blocks (ABBs)

Object representation of product-independent analytical engineering concepts

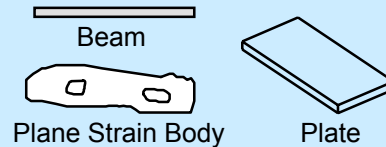
Analysis Primitives

- Primitive building blocks

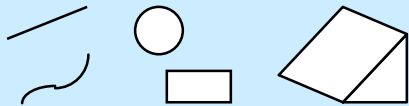
Material Models



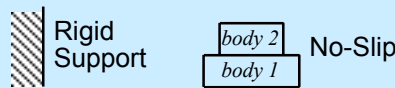
Continua



Geometry



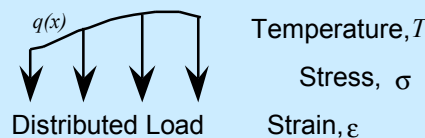
Interconnections



Discrete Elements



Analysis Variables

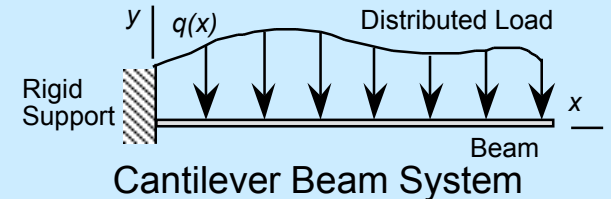


Analysis Systems

- Containers of ABB "assemblies"

Specialized

- Predefined templates



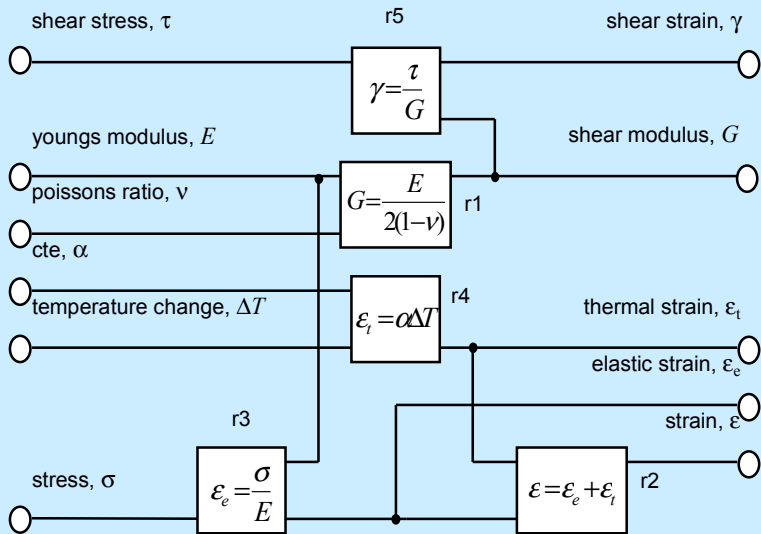
General

- User-defined systems

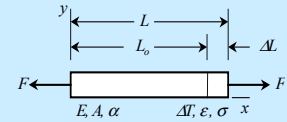
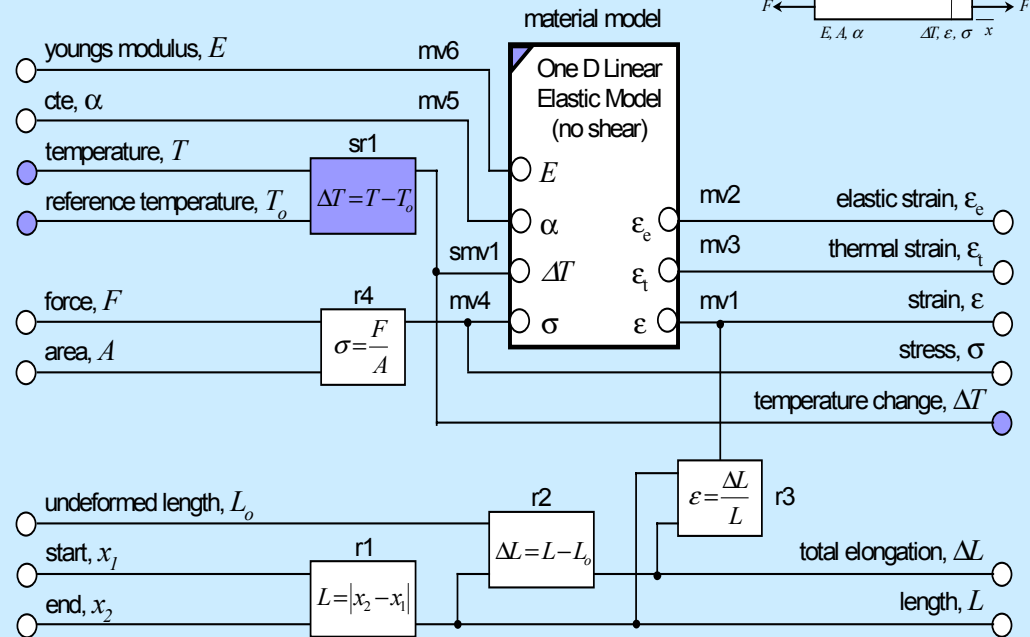


Primitive ABBs

1D Linear Elastic Model



Extensional Rod

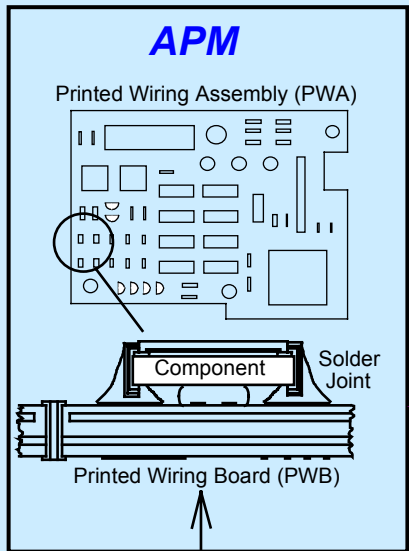


Usage by Flap Link Model

Multi-Representation Architecture for Design-Analysis Integration

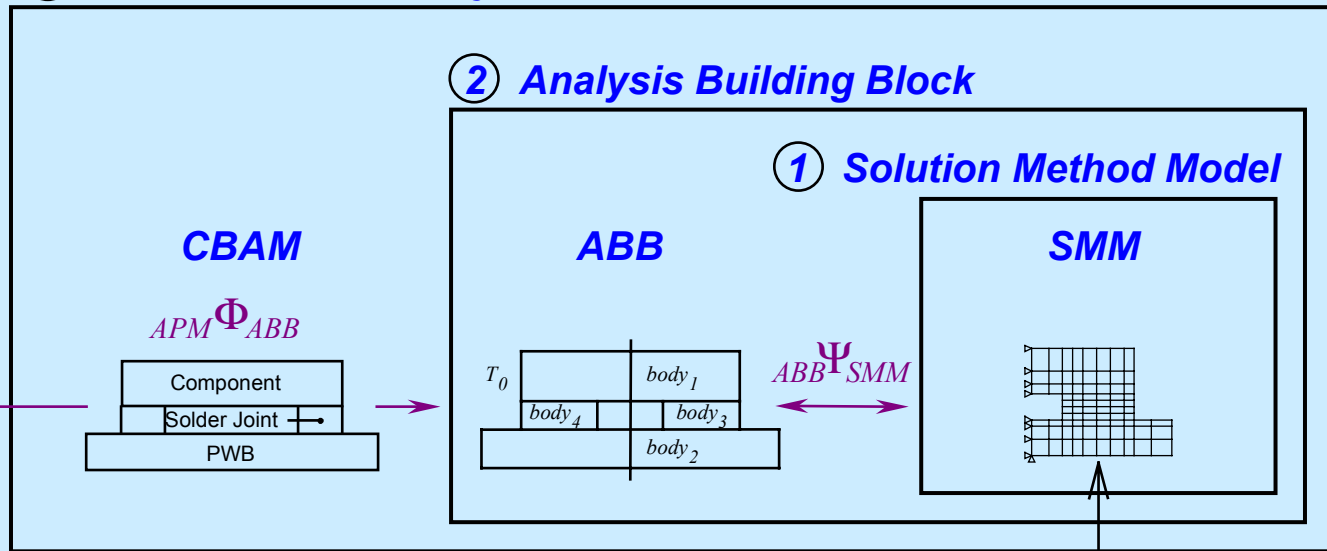


③ Analyzable Product Model



Design Tools

④ Context-Based Analysis Model



Solution Tools

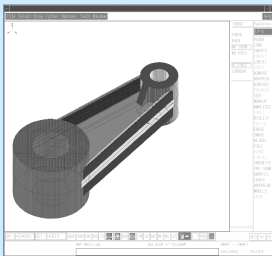
Analyzable Product Models (APMs)

Provide advanced access to design data needed by diverse analyses.

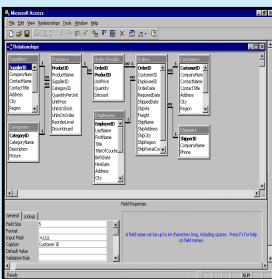
Design Applications

Analysis Applications

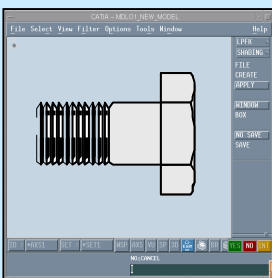
Solid Modeler



Materials Database

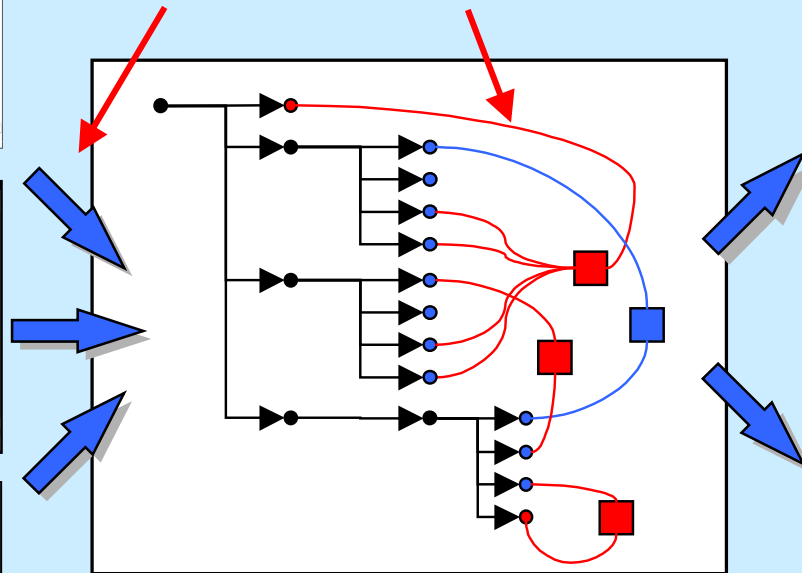


Fasteners Database



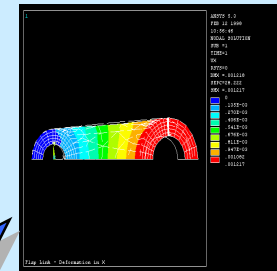
Combine information

Add reusable multifidelity idealizations

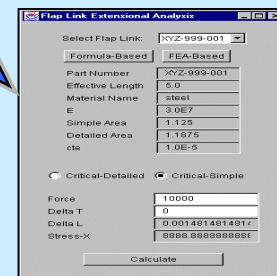


Analyzable Product Model (APM)

Support multidirectionality



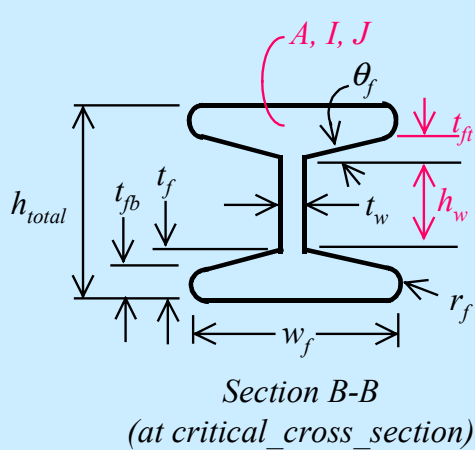
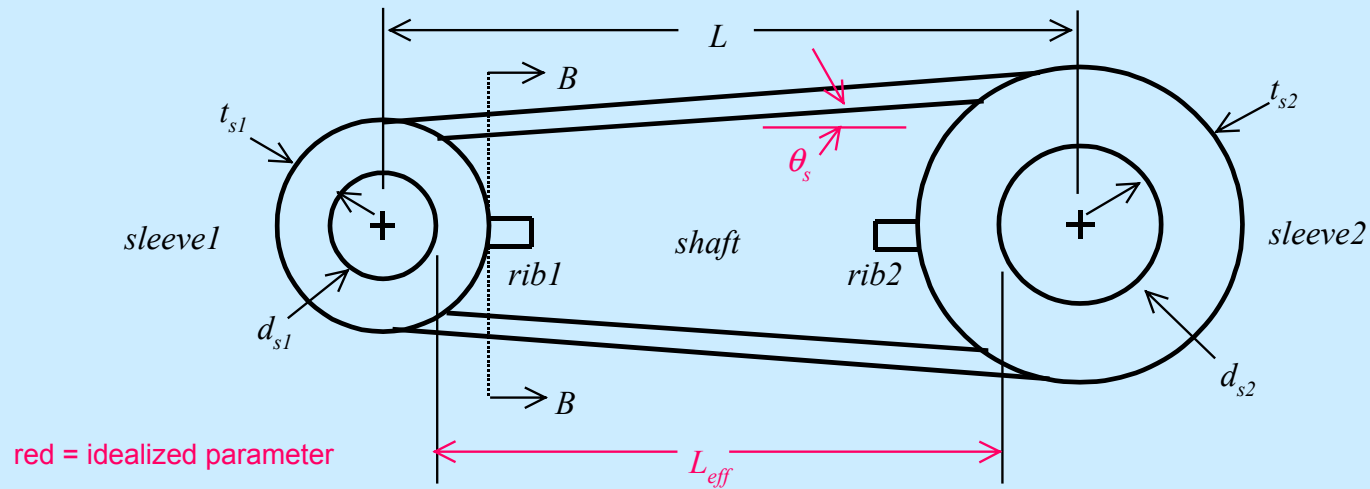
FEA-Based Analysis



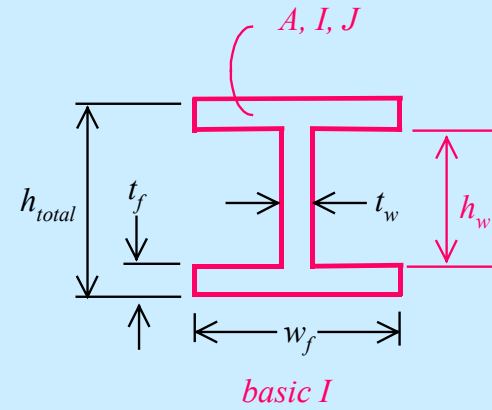
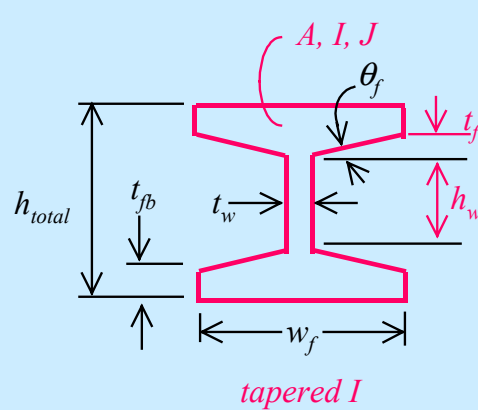
Formula-Based Analysis

Flap Link Geometric Model

(with idealizations)



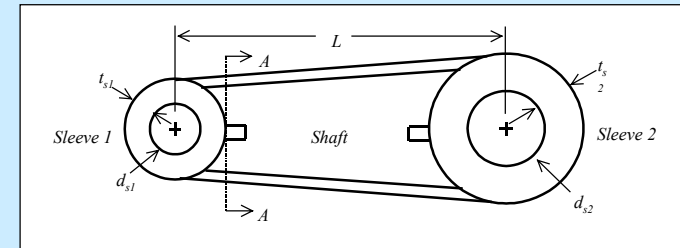
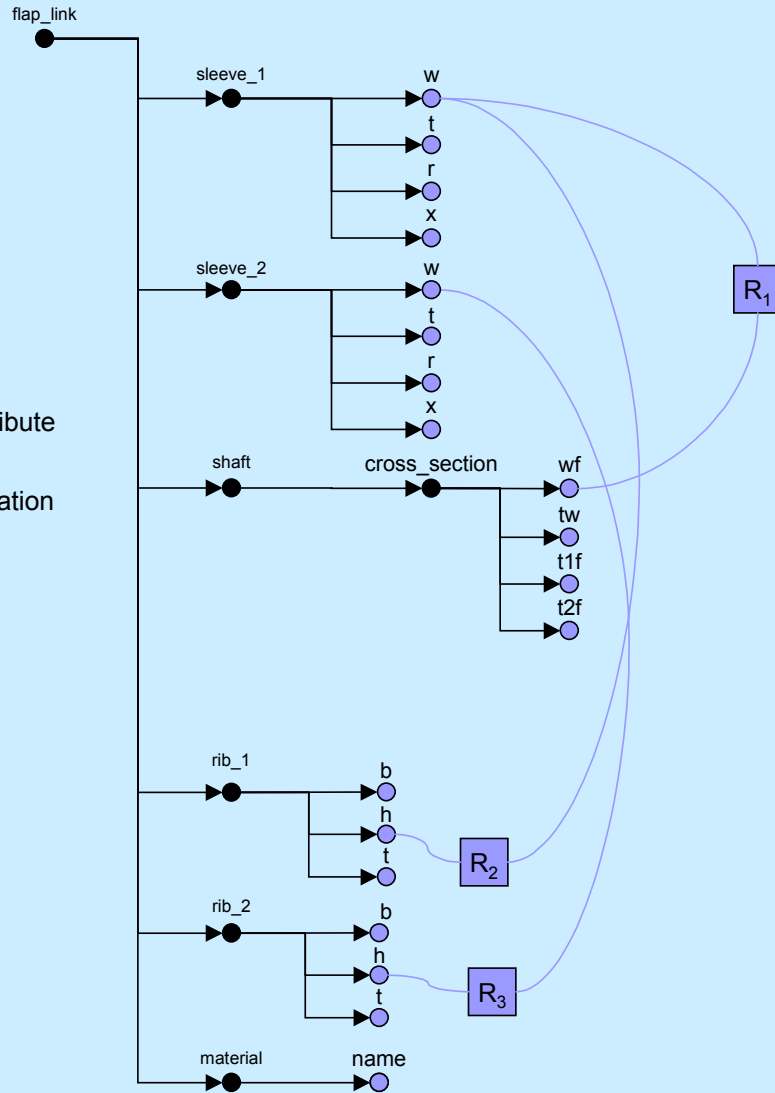
Detailed Design



Multifidelity Idealizations

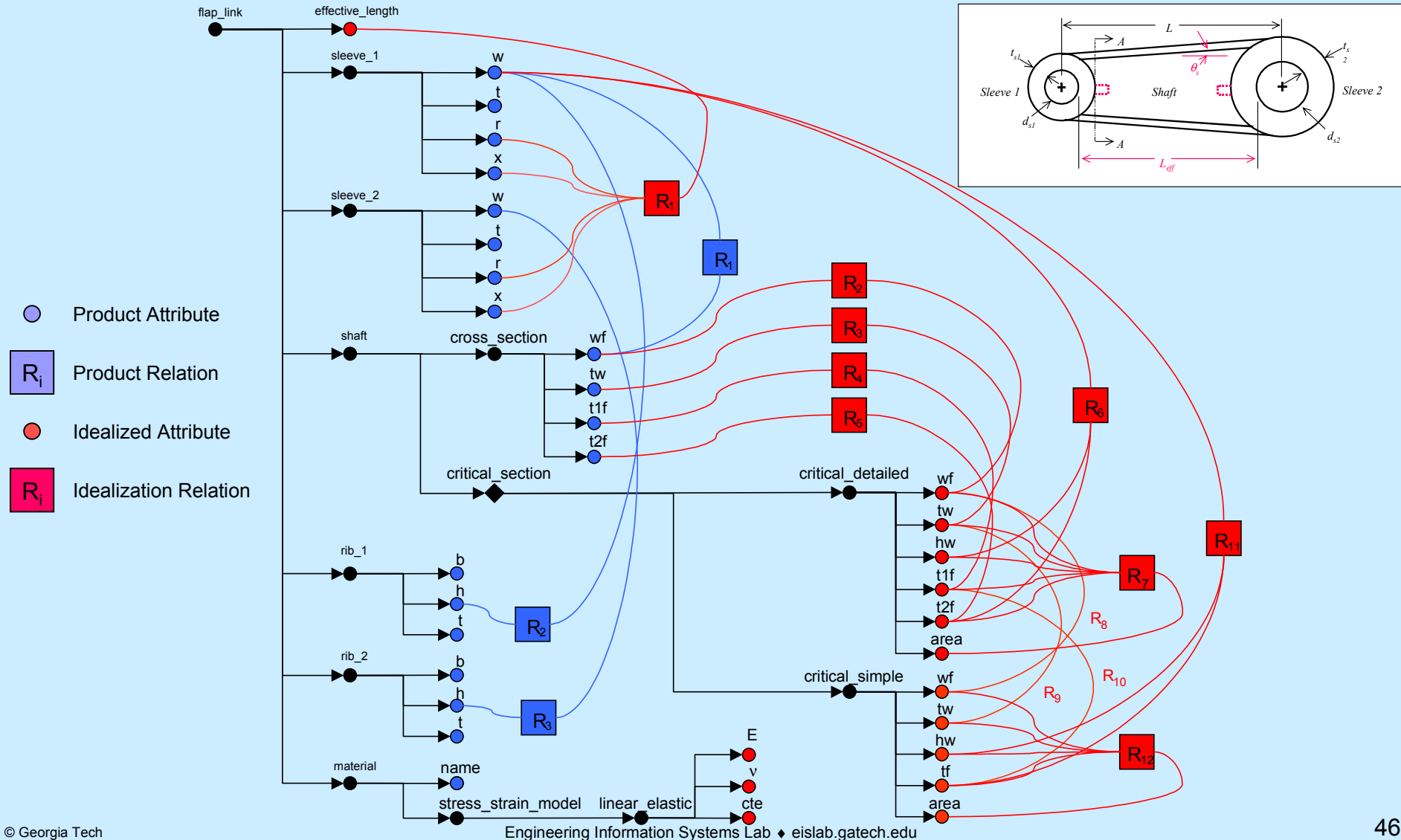
Flap Linkage Example

Manufacturable Product Model (MPM) = Design Description

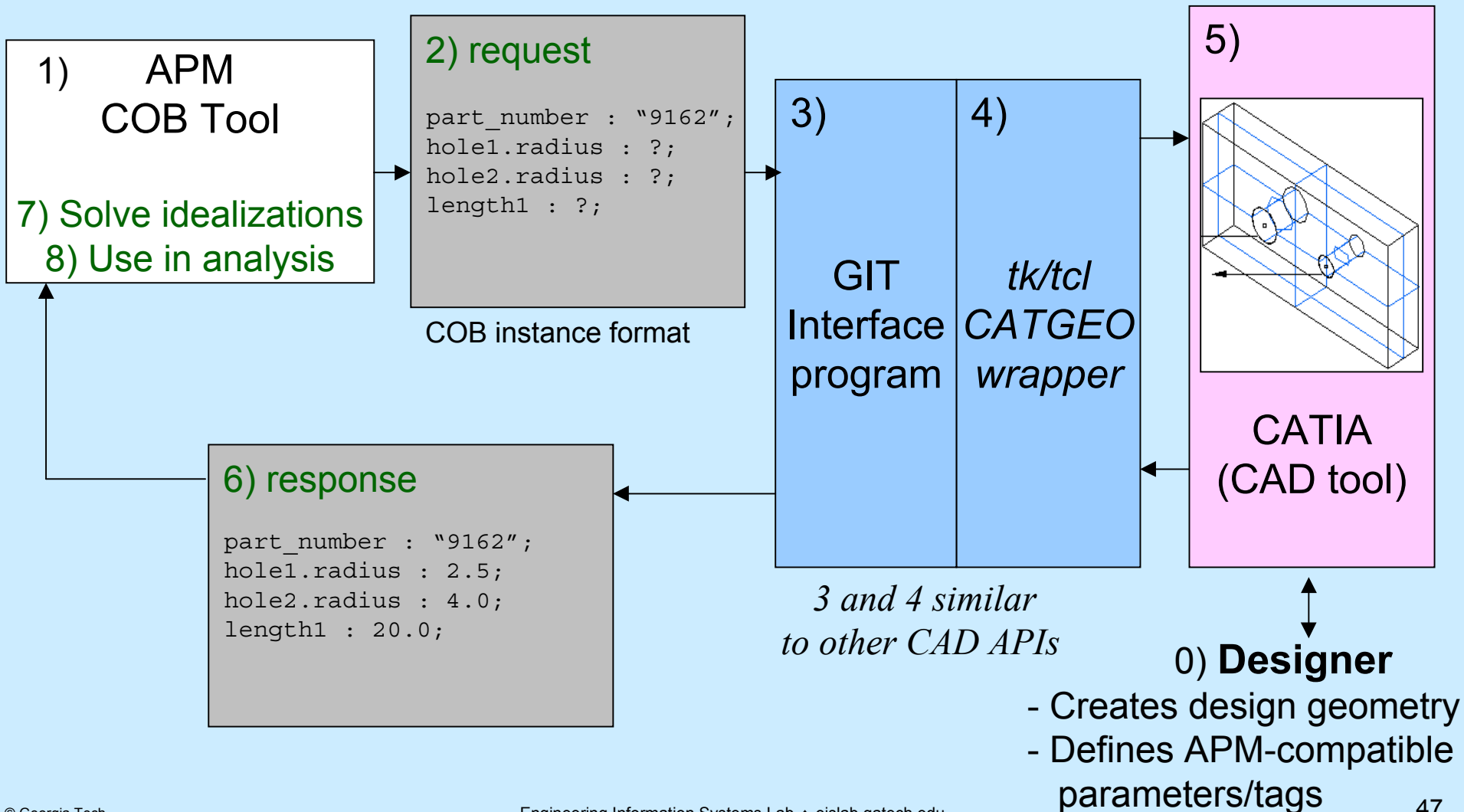


Flap Linkage Example

Analyzable Product Model (APM) = MPM Subset + Idealizations



APM Interface with Tagged CAD Models

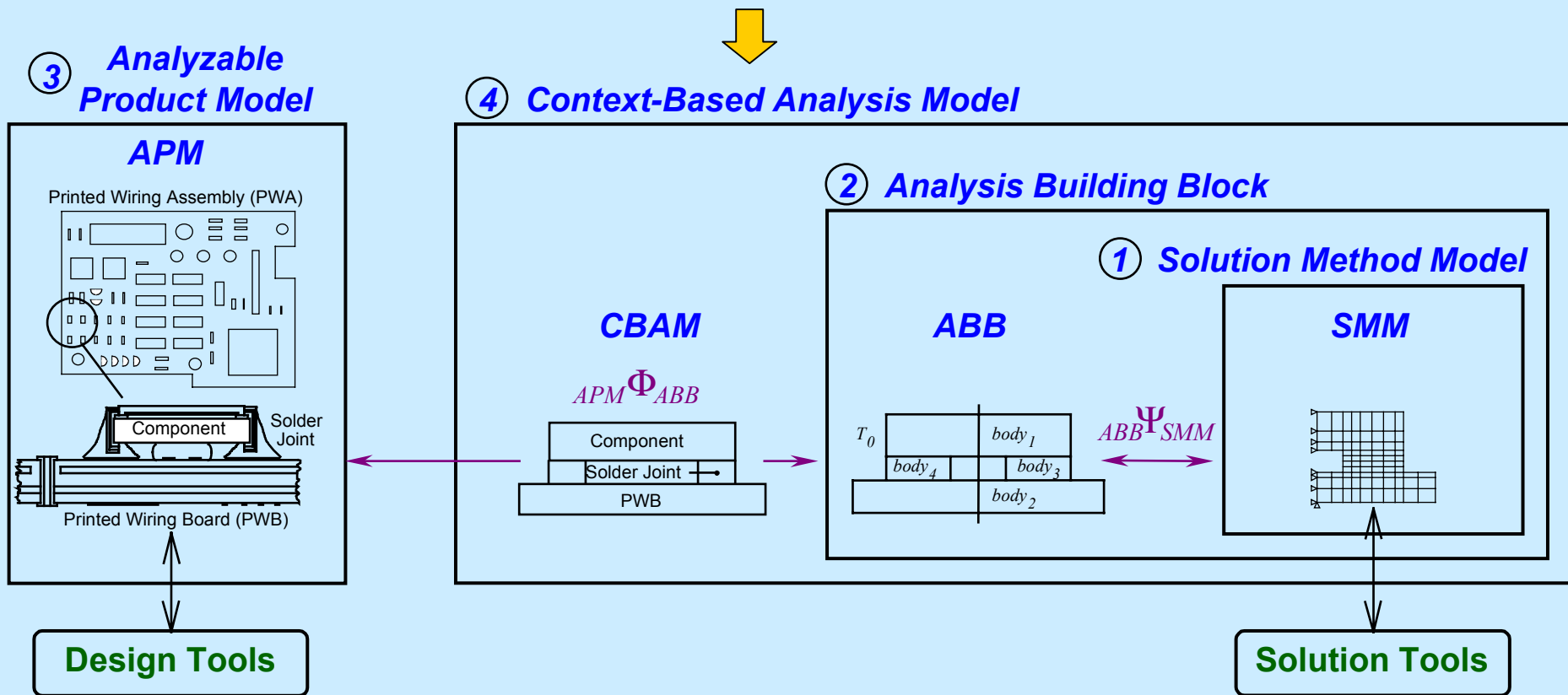


Flap Link Tagging

The image shows a CAD software window with a technical drawing of a flap link. The drawing includes a top view and a side view. Key dimensions and labels are as follows:

- Top View:** Shows two circular holes. The top hole has an outer diameter labeled $\varnothing 1$ and an inner diameter labeled $\varnothing 2$. The bottom hole has an outer diameter labeled $\varnothing 2.7$ and an inner diameter labeled $\varnothing 1.5$.
- Side View:** Shows the link's profile. The total length is labeled as 6.25. The distance between the centers of the two holes is labeled as $inter_axis_length$. The thickness of the link is labeled as 2.5.
- Labels:** Blue text labels include `sleeve2.inner_diameter` pointing to the inner diameter of the top hole, `sleeve2.width` pointing to the thickness of the link, and `inter_axis_length pointing to the distance between hole centers.`
- Angle:** An angle of 3.2102° is indicated between the top hole's axis and a horizontal reference line.
- Software Interface:** The window title bar includes "File Select View Filter Options Tools Window" and "Help". A "DIMENS" palette is open on the right, listing various dimensioning tools like CREATE, MODIFY, ISOLATE, STANDARD, VERIFY, DISTANCE, HORIZONTAL, VERTICAL, NORMAL, PARALLEL, NO TOL, STD TOL, and KEY TOL. The bottom status bar shows "SEL ELEM // YES:START PROCESS" and "DRAFT = *DRAFT".

Multi-Representation Architecture for Design-Analysis Integration



Tutorial Example: Flap Link Analysis Problems/CBAMs

Flap Link SCN

(2) Torsion Analysis

(1) Extension Analysis

- a. 1D Extensional Rod
- b. 2D Plane Stress FEA

1. Mode: **Shaft Tension**

2. BC Objects

Flaps down : $F = 10000$ lbs

3. Part Feature (idealized)

$L_{eff} = 5.0$ in **1020 HR Steel**

$A = 1.13$ in² $E = 30e6$ psi

$\sigma_{allowable} = 18000$ psi

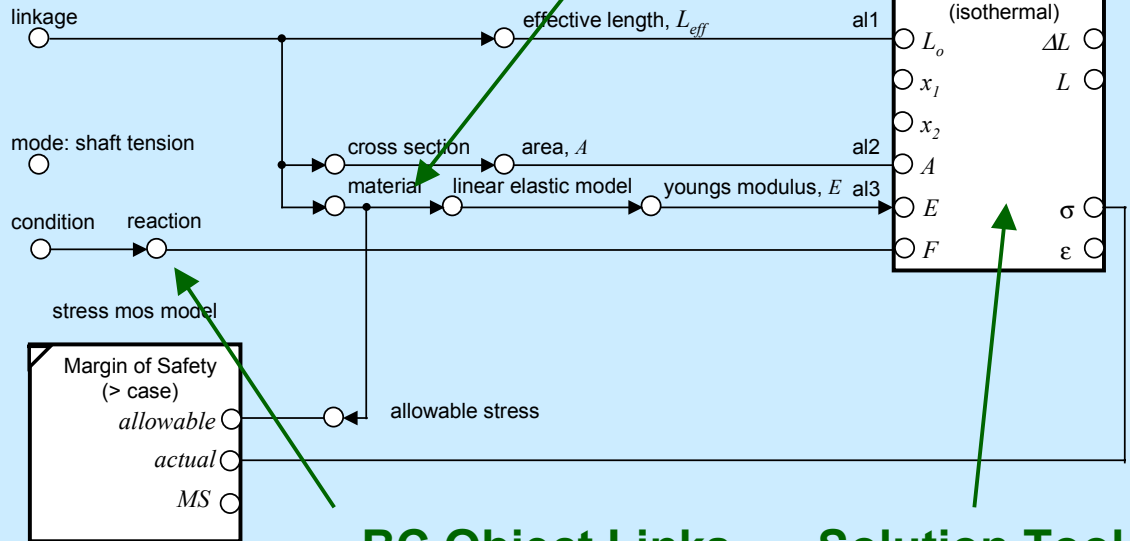
4. Analysis Calculations

$$\sigma = \frac{F}{A} \quad \Delta L = L_{eff} \frac{\sigma}{E}$$

5. Objective

$$MS = \frac{\sigma_{allowable}}{\sigma} - 1 = 1.03$$

(1a) Analysis Problem for 1D Extension Analysis



Pullable Views*

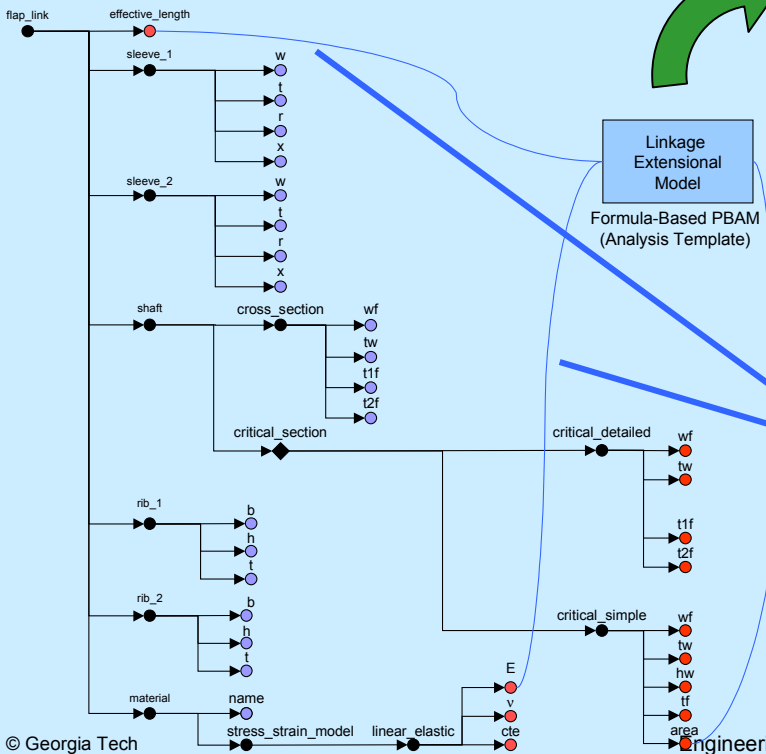
BC Object Links
(other analyses)*

Solution Tool
Links

* Boundary condition objects & pullable views are WIP*

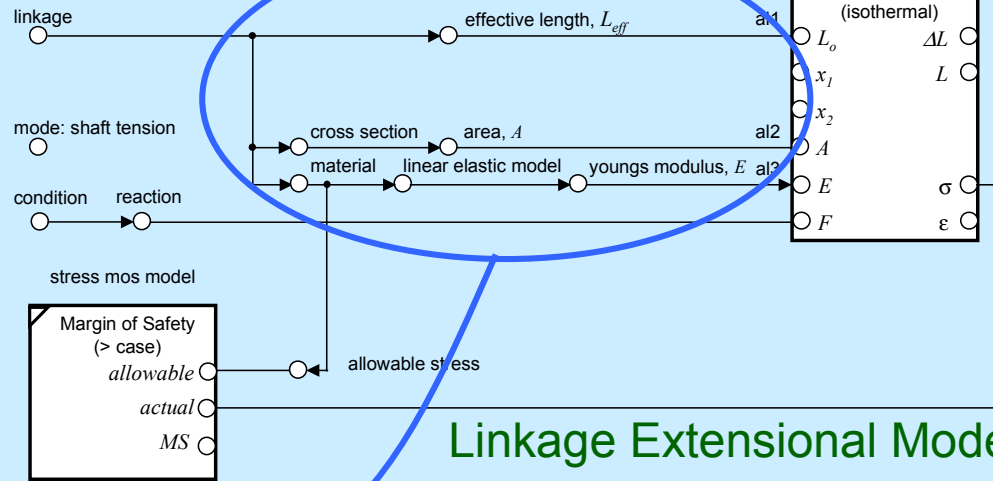
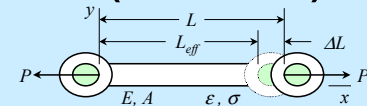
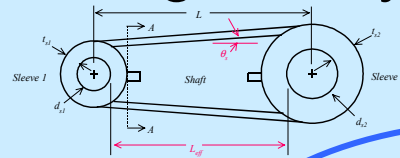
Analysis Template Usage of APM Idealized Attributes

Linkage APM



Linkage Extensional Model
Formula-Based PBAM
(Analysis Template)

Linkage Analysis Template (CBAM)



Linkage Extensional Model

Flap Linkage Extensional Model: Lexical COB Structure

```
COB link_extensional_model SUBTYPE_OF link_analysis_model;
DESCRIPTION
```

```
"Represents 1D formula-based extensional model.";
```

```
ANALYSIS_CONTEXT
```

```
PART_FEATURE
```

```
link : flap_link
```

```
BOUNDARY_CONDITION_OBJECTS
```

```
associated_condition : condition;
```

```
MODE
```

```
"tension";
```

```
OBJECTIVES
```

```
stress_mos_model : margin_of_safety_model;
```

```
ANALYSIS_SUBSYSTEMS */
```

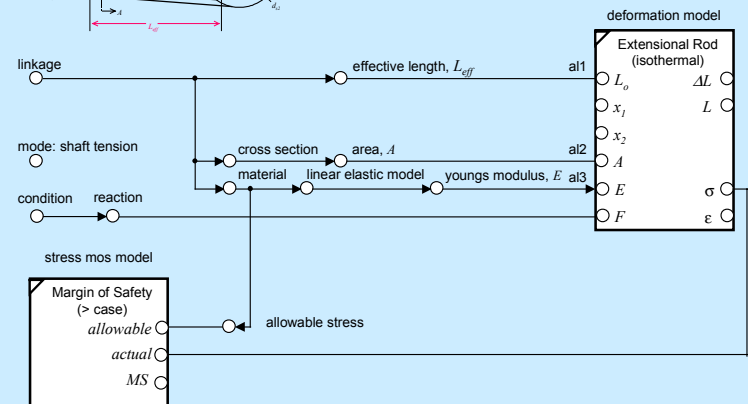
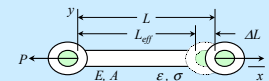
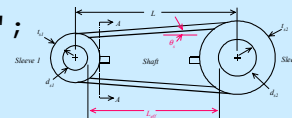
```
deformation_model : extensional_rod_isothermal;
```

```
RELATIONS
```

```
al1 : "<deformation_model.undeformed_length> == <link.effective_length>";
al2 : "<deformation_model.area> == <link.shaft.critical_cross_section.basic.area>";
al3 : "<deformation_model.material_model.youngs_modulus> ==
      <link.material.stress_strain_model.linear_elastic.youngs_modulus>";

al4 : "<deformation_model.material_model.name> == <link.material.name>";
al5 : "<deformation_model.force> == <associated_condition.reaction>";

al6 : "<stress_mos_model.allowable> == <link.material.yield_stress>";
al7 : "<stress_mos_model.determined> == <deformation_model.material_model.stress>";
END_COB;
```



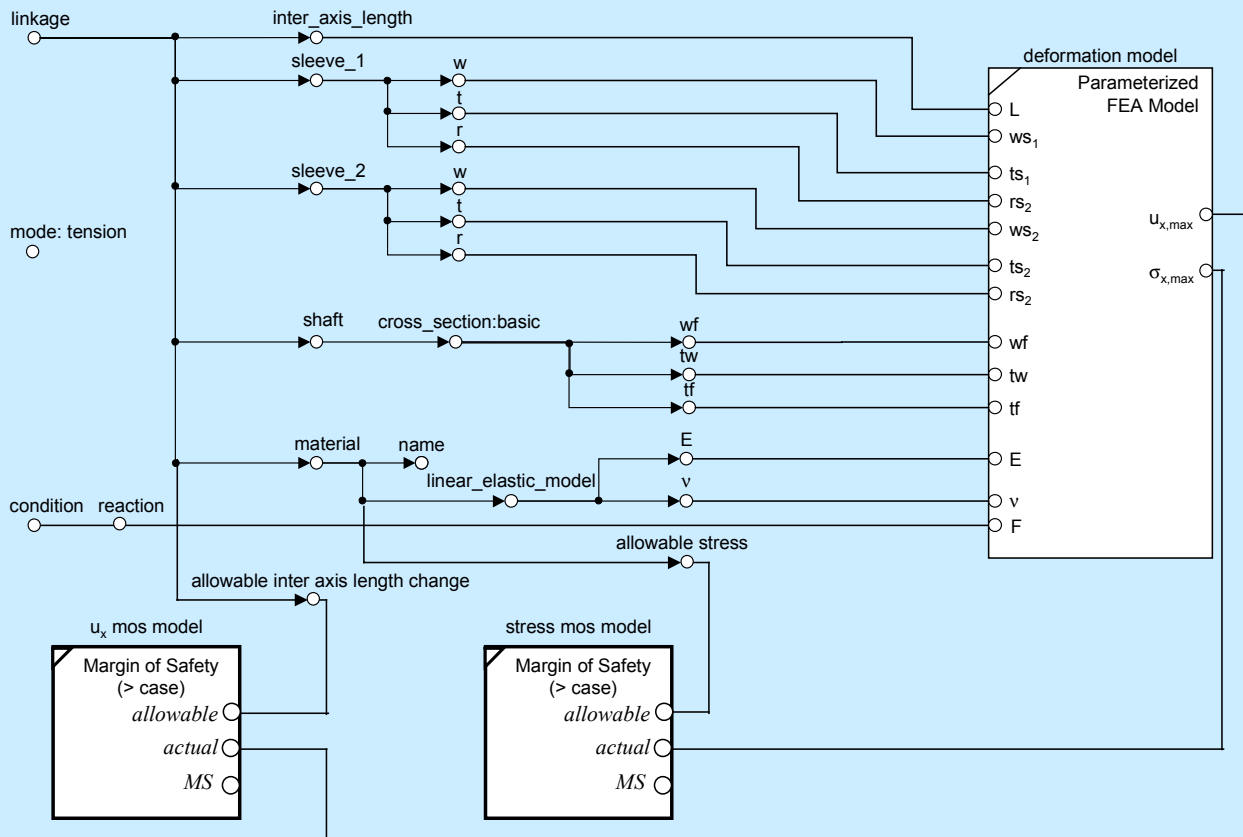
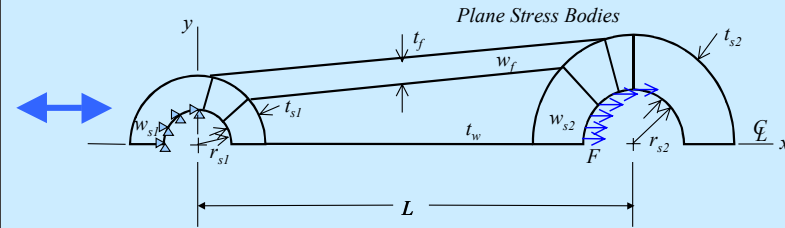
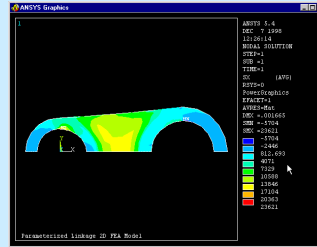
Desired categorization of attributes is shown above (as manually inserted) to support pullable views.

Categorization capabilities is a planned XaiTools extension.

FEA-based Analysis Subsystem

Used in Linkage Plane Stress Model (2D Analysis Problem)

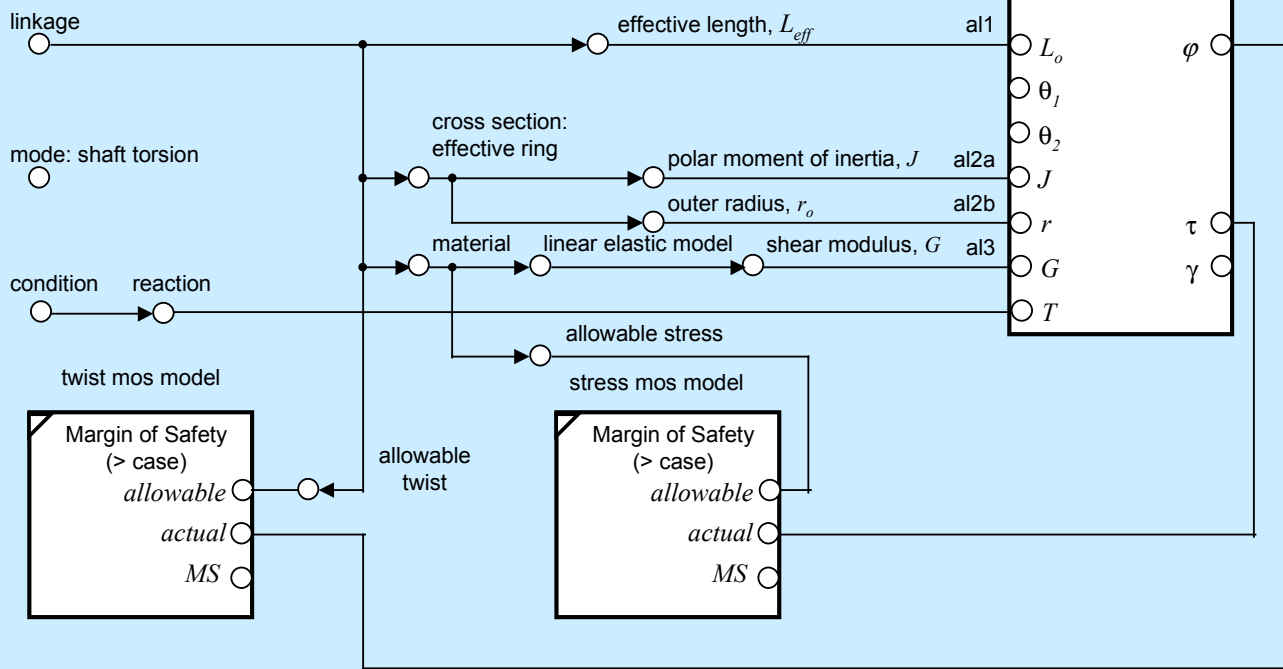
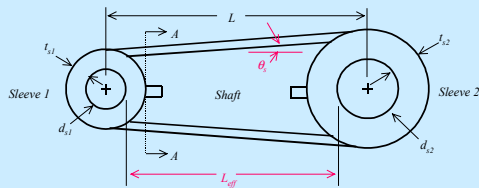
Higher fidelity version
vs. Linkage Extensional Model



Name	Symbol	Type	Input	Values
root		link_plane_stress_model		
link		link_plane_stress_model		
part_number		STRING	Input	"NYZ-510"
description		STRING	Input	"flap link type 5"
designer		STRING	Input	"J. Smrtn"
material		material		
origin		coordinate		
inter_axis_length		REAL	Input	6.25
sleeve1		sleeve		
width	w	REAL	Input	2
outer_diameter		REAL	Input	2
inner_diameter		REAL	Input	1
wall_thickness	t	REAL	Output	0.5
origin		coordinate		
hole		hole		
sleeve2		sleeve		
shaft		tapered_beam		
effective_length	L-sub>eff</sub>	REAL	Output	5
rib1		rib		
rib2		rib		
mx_mos_model		margin_of_safety_model		
margin_of_safety	MS	REAL	Output	-0.23797207632
allowable		REAL	Output	18,000
determined		REAL	Output	23,621.18164
ux_mos_model		margin_of_safety_model		
margin_of_safety	MS	REAL	Output	2.003021219528
allowable		REAL	Output	0.005
determined		REAL	Output	0.0016649899
associated_condition		condition	Input	"flaps down"
description		STRING	Input	10,002
reaction		REAL	Input	10,002
deformation_model		link_plane_stress_abb		
ex		REAL	Output	30,000,000
nuxy		REAL	Output	0.3
l		REAL	Output	5
suet		REAL	Output	?

Flap Linkage Torsional Model

Diverse Mode (Behavior) vs. Linkage Extensional Model



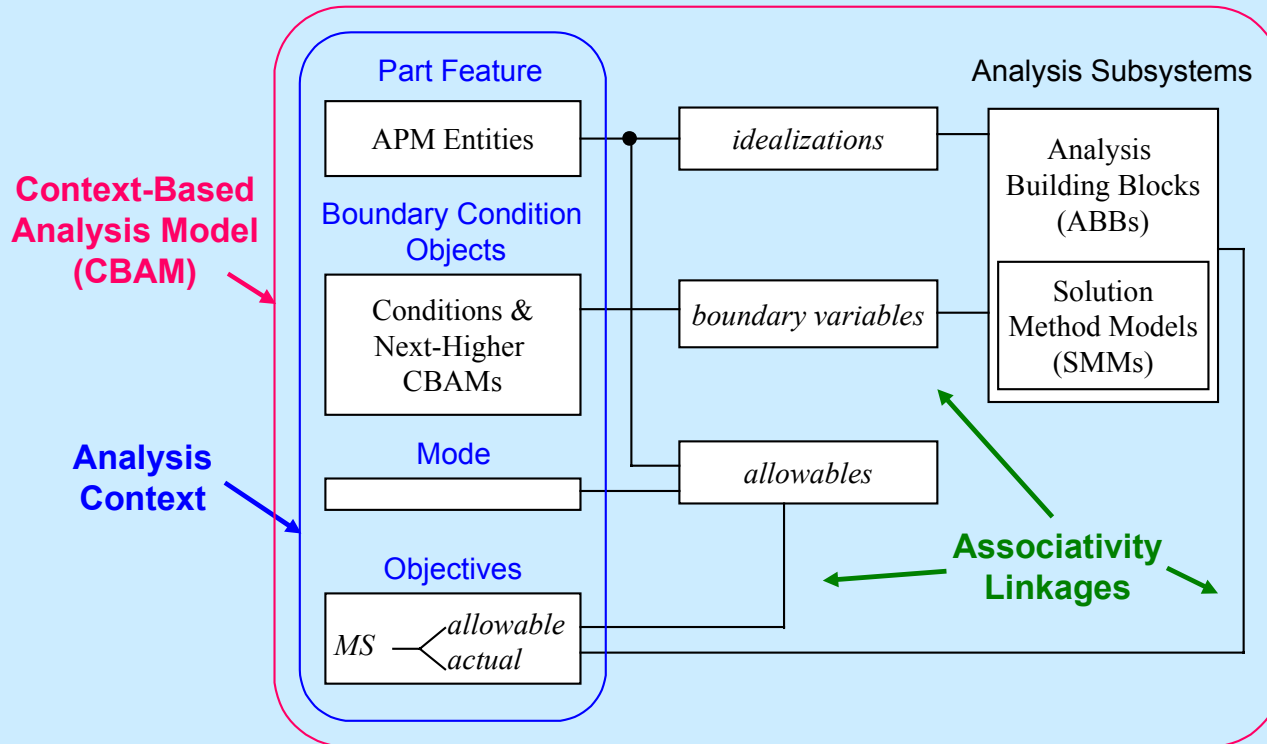
link_torsional_model

Name	Symbol	Type	Input	Values	
root		link_torsional_model			
link		flap_link			
part_number		STRING	Input	"XYZ-510"	
description		STRING	Input	"flap link type 5"	
designer		STRING	Input	"J. Smith"	
material		material			
allowable_twist_factor		REAL	Input	0.001	
allowable_inter_axis_length_C<sub>...>		REAL	Input	0.001	
origin		coordinate			
inter_axis_length		REAL	Input	6.25	
sleeve1		sleeve			
sleeve2		sleeve			
shaft		tapered_beam			
effective_length		REAL	Output	5	
allowable_twist		REAL	Output	0.005	
rib1		rib			
rib2		rib			
allowable_inter_axis_length_C<sub>...>		REAL	Output	0.005	
associated_condition		condition			
description		STRING	Input	"2G drive"	
reaction		REAL	Input	5,000	
stress_mos_model		margin_of_safety_model			
allowable		REAL	Output	18,000	
determined		REAL	Output	4,703.115814226	
margin_of_safety	MS	REAL	Output	2.82725	
twist_mos_model		margin_of_safety_model			
allowable		REAL	Output	0.005	
determined		REAL	Output	0.002139917695	
margin_of_safety	MS	REAL	Output	1.336538461538	
deformation_model		torsional_rod			
theta_start		θ<...>	REAL	Output	No value
theta_end		θ<...>	REAL	Output	No value
twist		φ<...>	REAL	Output	0.002139917695
torque	T	REAL	Output	5,000	
radius	r	REAL	Output	0.951280052281	

deformation_model (torsional_rod)

Name	Relation	Active
r1	<twist> == <theta_end> - <theta_start>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
r2	<material_model.shear_strain> == <twist> * <radius> / <undeformed_length>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
r3	<material_model.shear_stress> == <torque> * <radius> / <polar_moment_of_inertia>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
r1	<material_model.temperature_change> == <temperature> - <reference_temperat...	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Major Types of Analysis Objects



Analysis Context

- Analysis specification (why vs. how)
- Definable during early planning stages

*analysis problem a.k.a: template,
context-based analysis model (CBAM),
analysis module*

CBAM = why + how


= Analysis Context

+ Analysis Subsystems (ABBs, etc.)

+ Associativity Linkages

- Can be new, reused, or adapted template
- Instance can contain one or more runs

Outline

- ◆ Analysis Integration Challenges
- ◆ Introduction to Constrained Objects (COBs)
- ◆ Overview of COB-based XAI
- ◆ Example Applications 
 - ◆ Electronic Packaging Thermomechanical Analysis
 - ◆ Aerospace Structural Analysis
- ◆ Summary

STEP AP 210

PWA/B Design Information

Physical

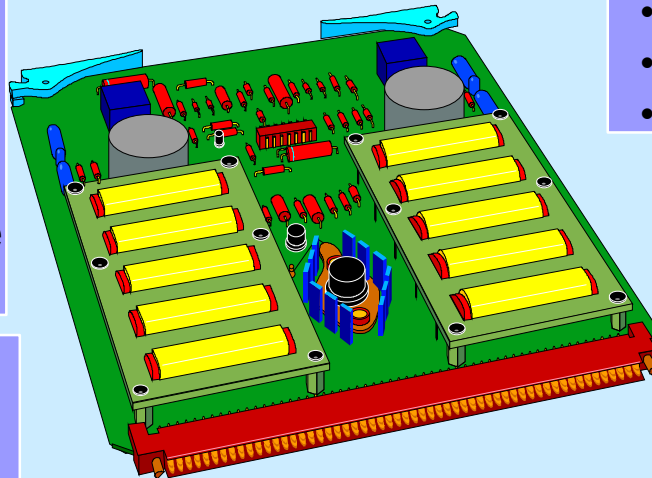
- Component Placement
- Bare Board Geometry
- Layout items
- Layers non-planar, conductive & non-conductive
- Material product

Geometry

- Geometrically Bounded 2-D Shape
- Wireframe with Topology
- Advanced BREP Solids
- Constructive Solid Geometry

Product Structure/Connectivity

- Functional
- Packaged



Requirements

- Design
- Allocation
- Constraints
- Interface

Part

- Functionality
- Termination
- Shape 2D, 3D
- Single Level Decomposition
- Material Product
- Characteristics

Configuration Mgmt

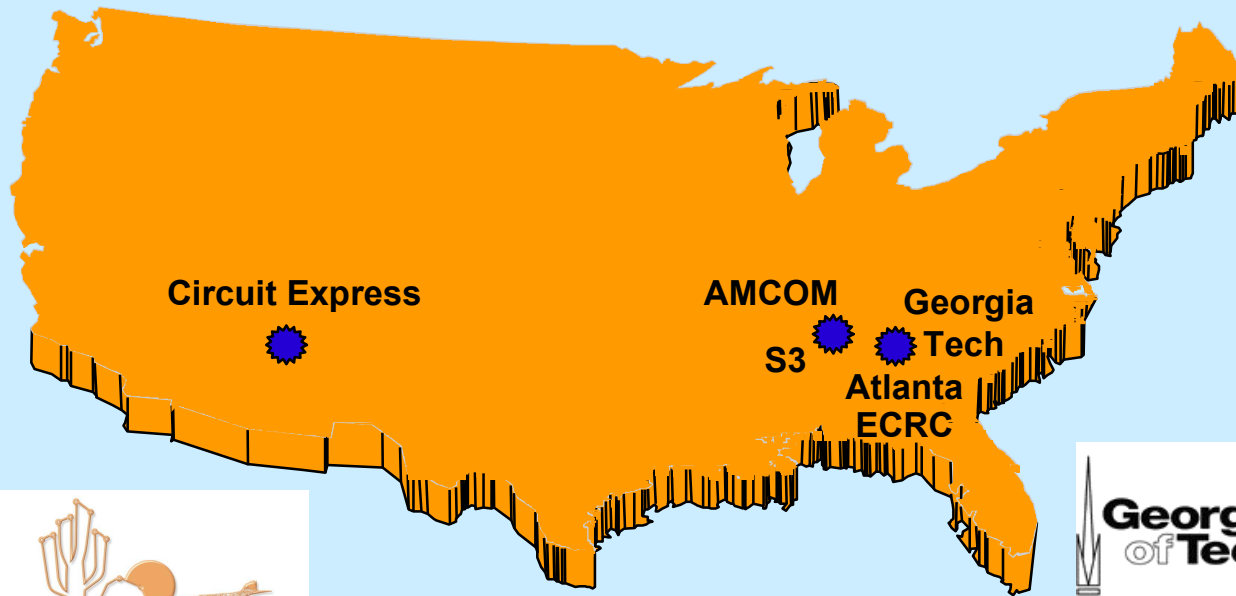
- Identification
- Authority
- Effectivity
- Control
- Requirement Traceability
- Analytical Model
- Document References

Technology

- Fabrication Design Rules
- Product Design Rules



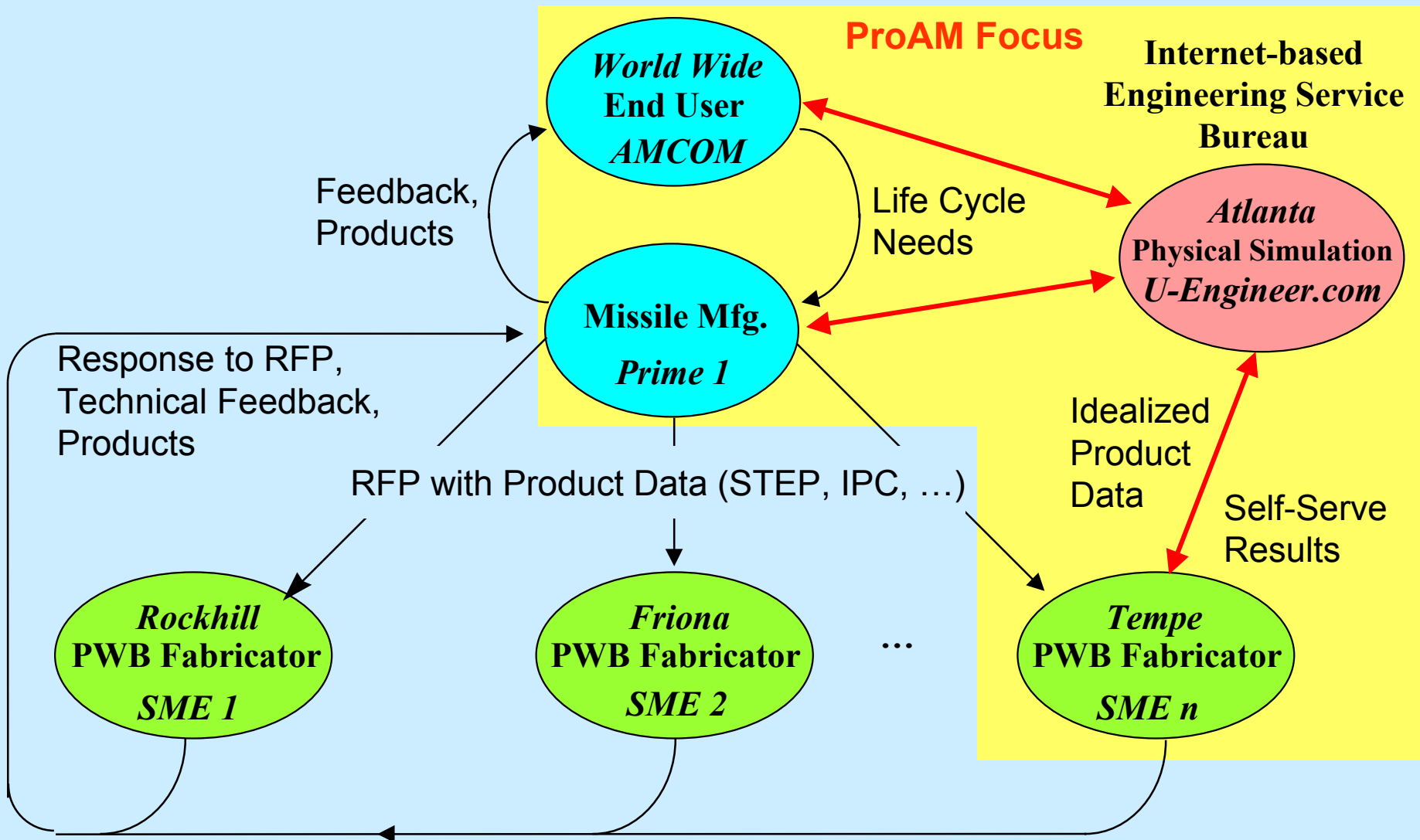
ProAM Technical Team





ProAM Focus

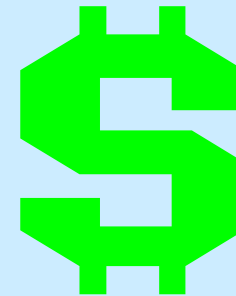
Highly Automated Internet-based Analysis Modules





Why Do SME Manufacturers Need Analysis?

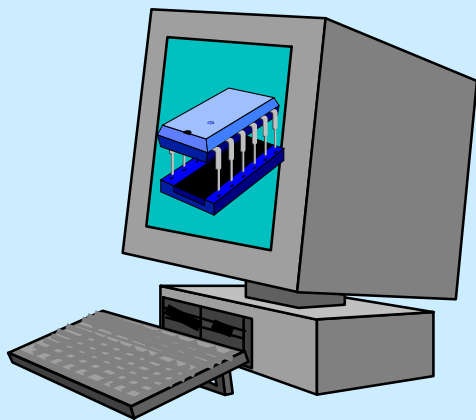
- ◆ Typically niche-experts
 - Precise mfg. process knowledge
 - Specialized product design knowledge (ex. PWB laminates)
- ◆ SME analysis needs
 - Product improvements (DFM)
 - Mfg. process troubleshooting
 - Mfg. process optimization
- ◆ More accurate data → Better analysis
- ◆ Bottom line drivers:
 - Higher Yields, Lower Cost,*
 - Better Quality, Fewer Delays*



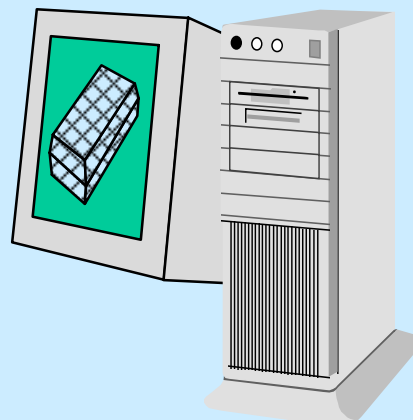
Barriers to SME Analysis

- ◆ Lack of awareness
- ◆ High costs of traditional analysis capability
 - Secondary: Specialized Software, Training, Hardware
 - Primary: Model Access/Development, Validation, Usage
- ◆ Lack of domain-specific integrated tools

Product Model



Analysis Model



Skilled Personnel





Internet-based Engineering Service Bureau (ESB) Tools

PWB Analysis Services (Bare Board)

PWB Layout Design

Post-Lamination Thickness	$f(x)$	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>	AP210
Coefficient of Thermal Bending	$f(x)$	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>	AP210

PWB Warpage Analysis

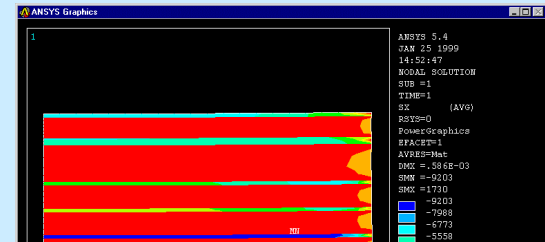
PTH Analysis Results

Input Variables

Drilled hole diameter, $d = 0.025$ inches
PWB Board thickness, $H = 0.0625$ inches
Barrel average plated thickness, $t_b = 0.0012$ inches
Barrel minimum plated thickness, $t_m = 0.001$ inches
Estimate of Plating Quality, $K_p = 6$
Reduction in local cross sectional area due to plating or drilling defects, $K_r = 10\%$

Change in temperature, $\Delta T = 200^\circ\text{C}$
Reference temperature (ambient), $T_{ref} = 25^\circ\text{C}$

Compression modulus
Coefficient of Thermal Expansion
Glass Transition Temp



PTH Deformation

One such structure is a bimaterial beam bending due to a uniform increase in temperature. Hence, we may wish to use this formula for a first order analysis of PWB Warpage.

Warpage $\delta = \frac{\alpha_b L^2 \Delta T}{t}$

In fact, if the analysis variables are selected correctly, it turns out that this simple model captures the maximum warpage wherever it occurs on the PWB! (For further details, examine our [Analysis Model Explanation](#) page.) For example, to model the board [Yeh et al](#) analyzed with FEM (illustrated at the top of the page) the figures for the 'input variables' are:

Undeformed (i.e. initial) Length $L = 276$ mm
Undeformed Thickness $t = 1.08$ mm
Temperature Change $\Delta T = 70^\circ\text{C}$ (from 25° to 95°C)
Specific Coefficient of Thermal Bending $\alpha_b = 1.10 \times 10^{-7}/^\circ\text{C}$ (from 25° to 95°C)

Since the formula does not predict the direction of the warpage, the resultant warpage figure (approximately 0.58 mm) represents the following PWB configurations: (warpage

PTH Geometry

t_b - Drilled hole radius: inches
 H - PWB board thickness: inches

PTH 'As Manufactured' Properties

t_b - Barrel average plated thickness: mils
 t_m - Barrel minimum plated thickness: mils
 K_p - Estimate of plating quality:
 K_r - Reduction in cross section due to local defects:

Analysis Model
IPC-D-279 Plated Through Hole

Results
Average Stress in the Maximum Strain in PTH Barrel Fatigue I

Please fill in the following properties of the PTH to be analyzed, then press the 'Continue Analysis' button. (Typical values have been provided.)

PWB Warpage Analysis

PWB Thermal Bending Model (1D Formulae)

PWB Total Diagonal	5.445181356024792
Thermal Bending Coef. (x,t)	3.496038E-7
Temperature Change	0
Warpage	0
Warpage Ratio	0
Margin of Safety	0

PWB Plane Strain Model (2D FEA)

Initial Temperature	0
Final Temperature	0
Temperature Change	0
FEA Min Elem Div	2
FEA Aspect Ratio	4
Max Stress %X	0
Local Warpage	0
Warpage Ratio	0
Margin of Safety	0

PWA/B Parameters

Description	Warning Module PWA
PWA Part #	ABC_9010
PWB Part #	ABC_9230
PWB Pre Lamination Thickness	0.0814
PWB Post Lamination Thickness	0.07303000000000001
PWB Total Width	3.7999999999999999
PWB Total Length	3.9
Allowable Warpage Ratio	0.0075

Calculate Results View Graphical Results

Analysis Documentation

Ready-to-Use Analysis Modules

Lower cost, better quality, fewer delays in supply chain



Paper-based IPC-D-279 Plated Through Hole Fatigue Analysis

Tedious to Use

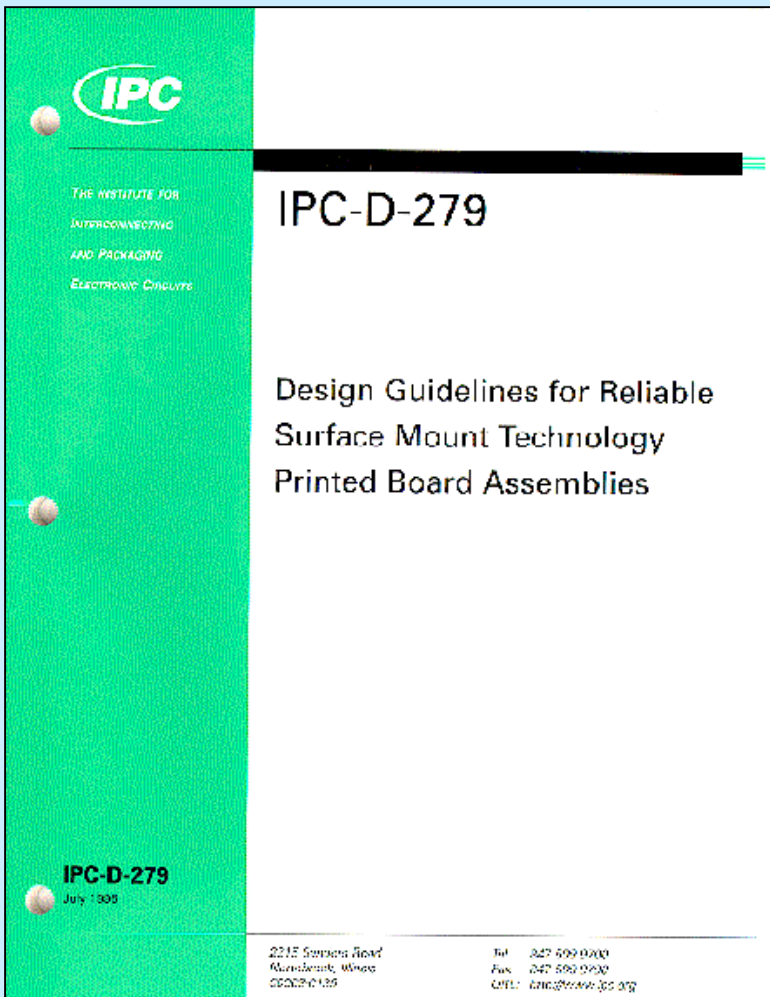
PTH/PTV Fatigue Life Estimation

$$\sigma_{avg} = \frac{\left[(\alpha_E - \alpha_{Cu}) \Delta T + S_y \cdot \frac{E_{Cu} - E_{Cu}'}{E_{Cu} \cdot E_{Cu}'} \right] \cdot A_E \cdot E_E \cdot E_{Cu}'}{A_E \cdot E_E + A_{Cu} \cdot E_{Cu}'}$$

$$\Delta \epsilon_{avg} = \frac{(\alpha_E - \alpha_{Cu}) \Delta T \cdot A_E \cdot E_E - S_y \cdot A_{Cu} \cdot \frac{E_{Cu} - E_{Cu}'}{E_{Cu}}}{A_E \cdot E_E + A_{Cu} \cdot E_{Cu}'}$$

$$N_f^{-0.6} D_f^{0.75} + 0.9 \frac{S_u}{E} \left[\frac{e^{D_f}}{0.36} \right]^{0.1785 \log \frac{10^5}{N_f}} - \Delta \epsilon = 0$$

$$N_f(x\%) = N_f(50\%) \left[\frac{\ln(1 - 0.01x)}{\ln(0.5)} \right]^{\frac{1}{\beta}}$$





Product Data-Driven IPC-D-279 PTH Analysis Module

Easier to Use

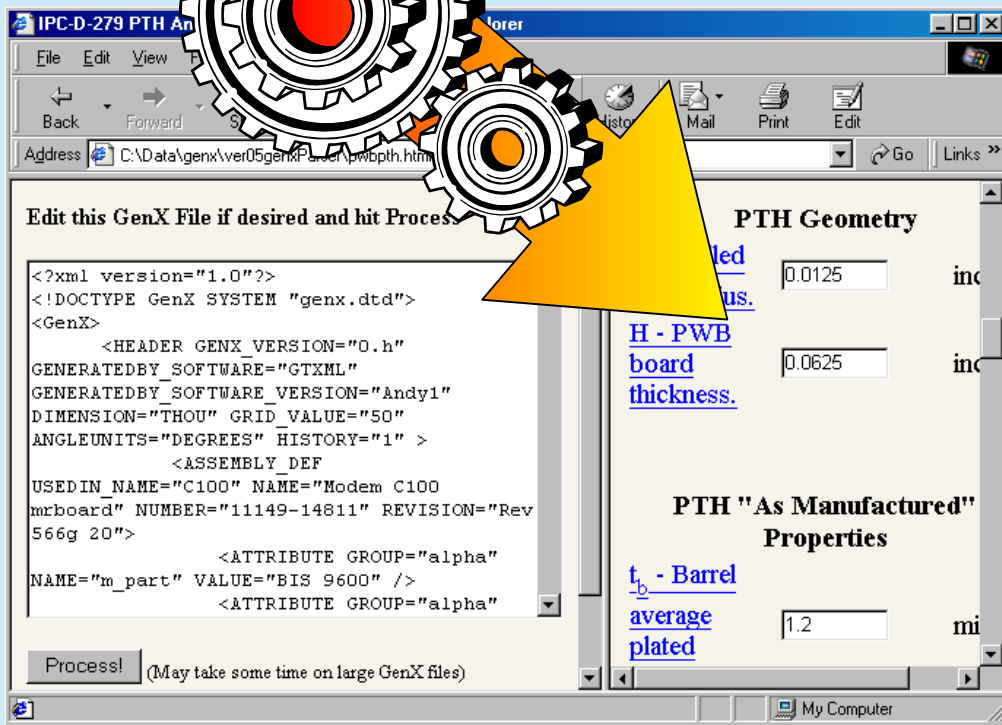
<?XML!> GenCAM/GenX



Xparse

JavaScript
parsing

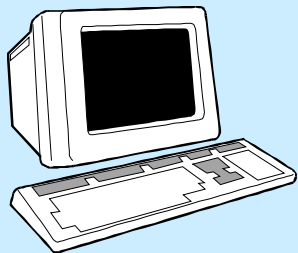
- ◆ Data Driven aspect: Web
 - + Local Browser Compu
 - + Less Errors than manu
 - + Exhaustive search
 - + Data Compression (e.g. 100x)
 - + Security



Analysis Data Flow

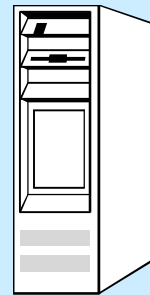
Web-based Approach

**SME
Client**



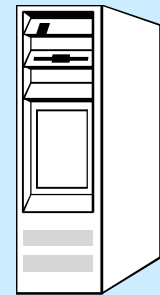
Pentium PC
Web Browser

**ESB Web
Server**

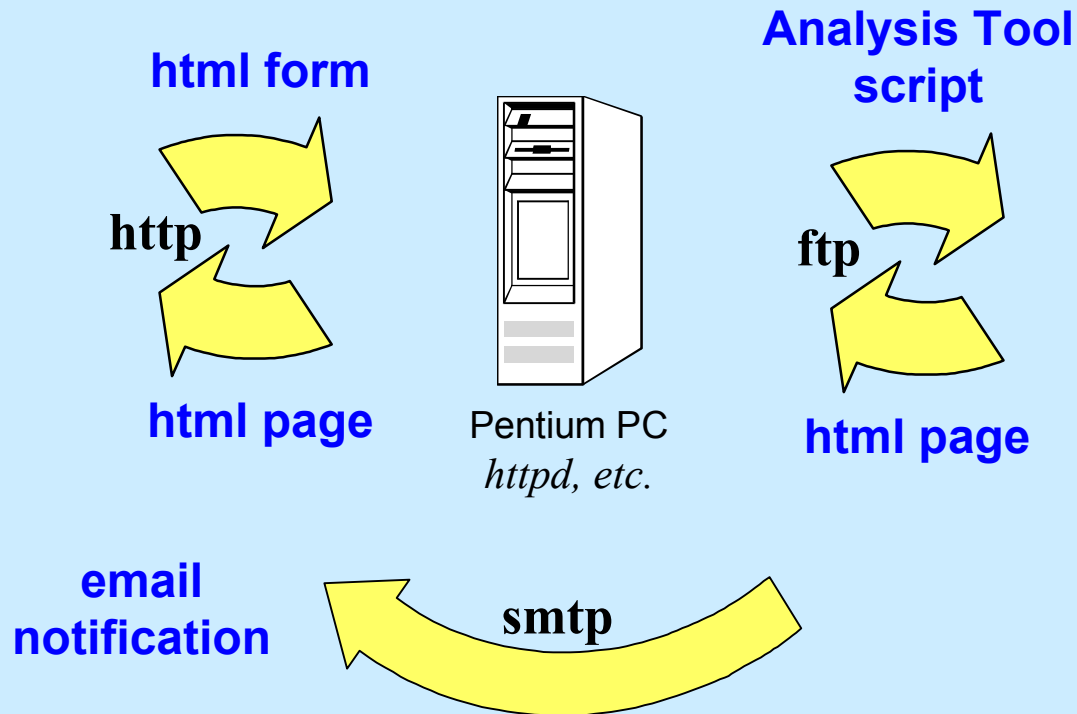


Pentium PC
httpd, etc.

**ESB Analysis
Server**



Sun SPARCstation
Mathematica



ESB Analysis Module Catalogs & Documentation

PWB Analysis Services (Bare Board)

PWB Layup Design

| | | | | | | | |
|--------------------------------|---|--------|----------------------------------|-----------------------|----------------------------------|-------------------------------------|-------|
| Post-Lamination Thickness | - | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |
| Coefficient of Thermal Bending | - | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |

PWB Warpage Analysis

| | | | | | | | |
|---|----|--------|----------------------------------|-----------------------|----------------------------------|-------------------------------------|-------|
| Thermal Bending Model | 1D | $f(x)$ | <input type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |
| Classical Lamina Theory Model | 2D | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | |
| Plane Strain Model (Material Variation) | 2D | | <input type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |

PTH Deformation & Fatigue Analysis

| | | | | | | | |
|--|----|--------|------------------------------------|----------------------------------|----------------------------------|-------------------------------------|------|
| IPC 279 Model (cylinder/Coffin-Manson) | 1D | $f(x)$ | <input checked="" type="radio"/> P | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Mirman Beam Model | 1D | $f(x)$ | <input checked="" type="radio"/> P | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Axisymmetric Model | 2D | | <input checked="" type="radio"/> | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Palmgren-Miner Model | - | $f(x)$ | <input type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | |

PWB Warpage - Netscape

Since the residual stresses which cause warpage are partly due to the coefficient of thermal expansion (CTE) mismatch between the materials in a PWB board, we may wish to search the [reference books](#) for other composite structures which warp due to mismatched CTEs.

One such structure is a bimaterial beam bending due to a uniform increase in temperature. Hence, we may wish to use this formula for a first order analysis of PWB Warpage.

PWB: Thermal Bending

$$\text{Warpage } \delta = \frac{\alpha_b L^2 \Delta T}{t}$$

In fact, if the analysis variables are selected correctly, it turns out that this simple model captures the maximum warpage wherever it occurs on the PWB! (For further details, examine our [Analysis Model Explanation page](#).) For example, to model the board [Yeh et al](#) analyzed with FEM (illustrated at the top of the page) the figures for the 'input' variables are:


- Undeformed (i.e. initial) Length $L = 276$ mm
- Undeformed Thickness $t = 1.08$ mm
- Temperature Change $\Delta T = 70$ °C (from 25° to 95°C)
- Specific Coefficient of Thermal Bending $\alpha_b = 1.10 \times 10^{-7}$ /°C (from 25° to 95°C)

Since the formula does not predict the direction of the warpage, the resultant warpage figure (approximately 0.58 mm) represents the following PWB configurations: (warpage



Analysis Modules Attributes

Solution Method - An indication of model computational cost.

$f(x)$ Formula Based
 Finite Element

Utility Ranking - A measure of analysis model validity.

 Demonstration
 Trends
 Magnitude Relative
 Absolute

A "P" suffix indicates the ranking is backed by physical measurements.

Tool Availability - A measure of implementation maturity.

 Concept
 Prototype
 Pilot
 Production


| Dimensionality | Solution Method | Utility Ranking | Availability | | | Supported Design Formats |
|----------------|-----------------|-----------------|------------------|----------------------|--------------|--------------------------|
| | | | Self - Serve Web | Self - Serve Toolkit | Full - Serve | |
| | | | | | | |

PWB Analysis Services (Bare Board)


PWB Layup Design

| | | | | | | | |
|--------------------------------|---|--------|----------------------------------|-----------------------|----------------------------------|-------------------------------------|-------|
| Post-Lamination Thickness | - | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |
| Coefficient of Thermal Bending | - | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |

PWB Warpage Analysis

| | | | | | | | |
|---|----|---|----------------------------------|-----------------------|----------------------------------|-------------------------------------|-------|
| Thermal Bending Model | 1D | $f(x)$ | <input type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |
| Classical Lamina Theory Model | 2D | $f(x)$ | <input checked="" type="radio"/> | <input type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | |
| Plane Strain Model (Material Variation) | 2D |  | <input type="radio"/> | <input type="radio"/> | <input checked="" type="radio"/> | <input checked="" type="checkbox"/> | AP210 |

PTH Deformation & Fatigue Analysis

| | | | | | | | |
|--|----|---|------------------------------------|----------------------------------|-----------------------|-------------------------------------|------|
| IPC 279 Model (cylinder/Coffin-Manson) | 1D | $f(x)$ | <input checked="" type="radio"/> P | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Mirman Beam Model | 1D | $f(x)$ | <input checked="" type="radio"/> P | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Axisymmetric Model | 2D |  | <input checked="" type="radio"/> | <input checked="" type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | GenX |
| Palmgren-Miner Model | - | $f(x)$ | | <input type="radio"/> | <input type="radio"/> | <input checked="" type="checkbox"/> | |

ESB Characteristics

◆ Self-serve analysis

- Pre-developed analysis modules presented in product & process contexts
- Available via the Internet
- Optionally standards-driven (STEP, GenCAM ...):
 - » Reduce manual data transformation & re-entry
 - » Highly automated plug-and-play usage
- Enabled by X-analysis integration technology

◆ Full-serve analysis as needed

◆ Possible business models:

(beyond ProAM scope)

- Pay-per-use and/or Pay-per-period



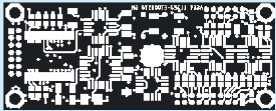
ProAM Design-Analysis Integration

Electronic Packaging Examples: PWA/B

Design Tools

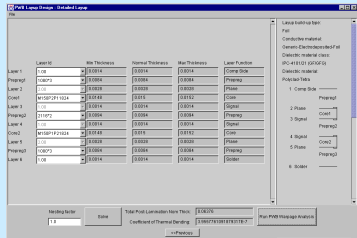
ECAD Tools

Mentor Graphics,
Accel*



PWB Layup Tool

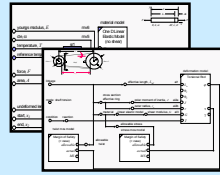
XaiTools PWA-B



Laminates DB



Materials DB



Modular, Reusable Template Libraries

STEP AP210,
GenCAM**,
PDF*

Analyzable Product Model



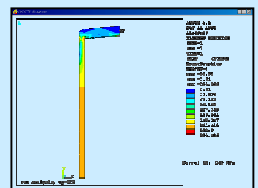
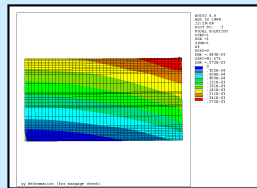
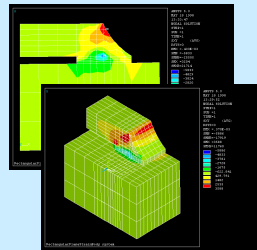
Analysis Modules (CBAMs) of Diverse Mode & Fidelity

XaiTools
PWA-B

Analysis Tools

General Math
Mathematica

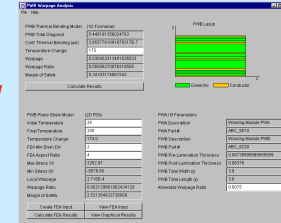
FEA Ansys



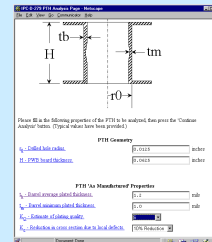
Solder Joint
Deformation* 1D,
2D,
3D



PWB
Warpage 1D,
2D

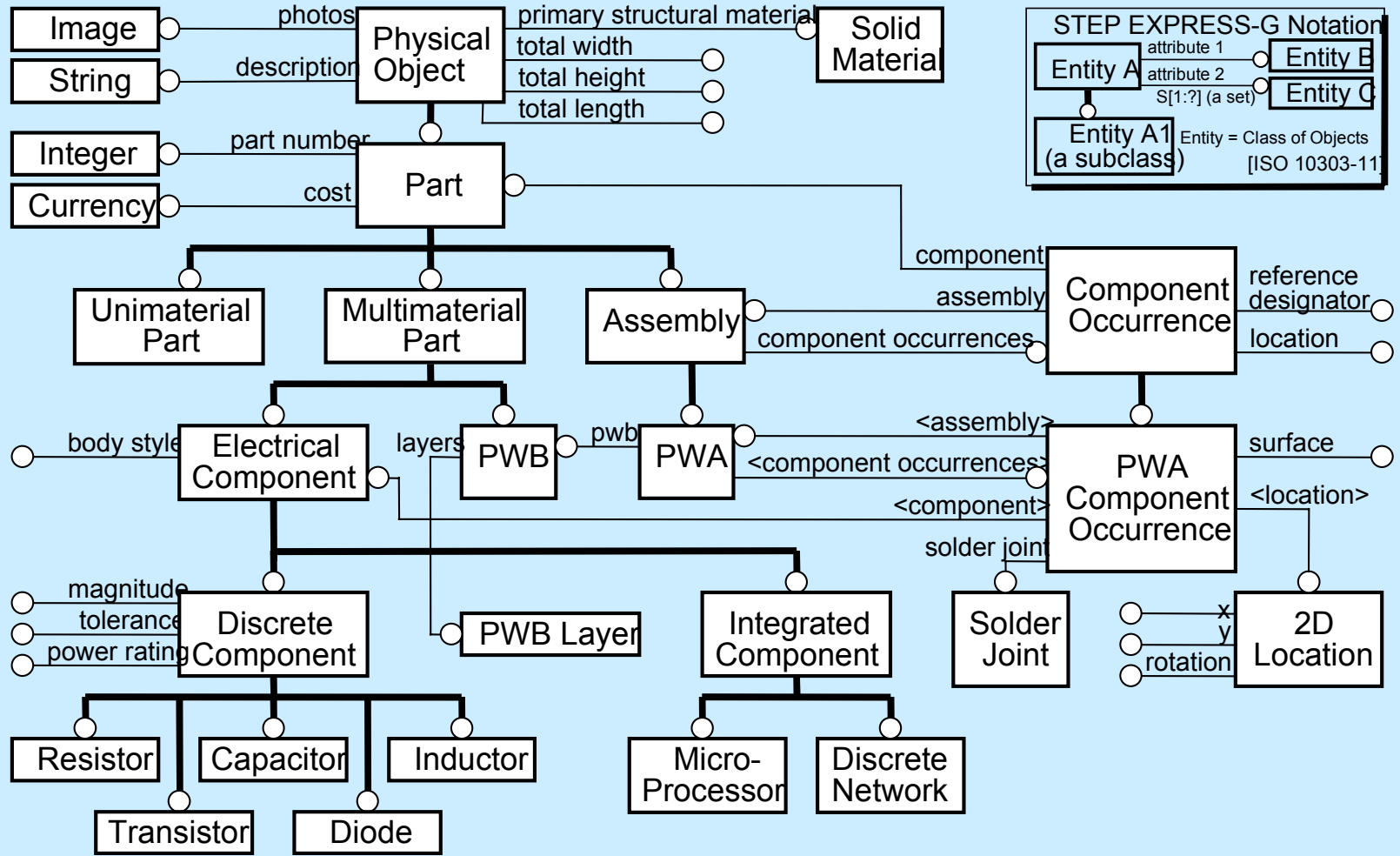


PTH
Deformation
& Fatigue** 1D,
2D



* = Item not yet available in toolkit (all others have working examples) ** = Item available via U-Engineer.com

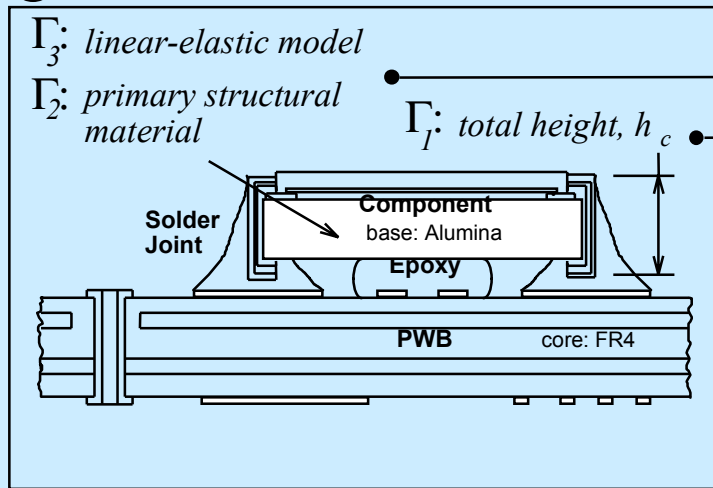
PWA/B Analyzable Product Model (partial)



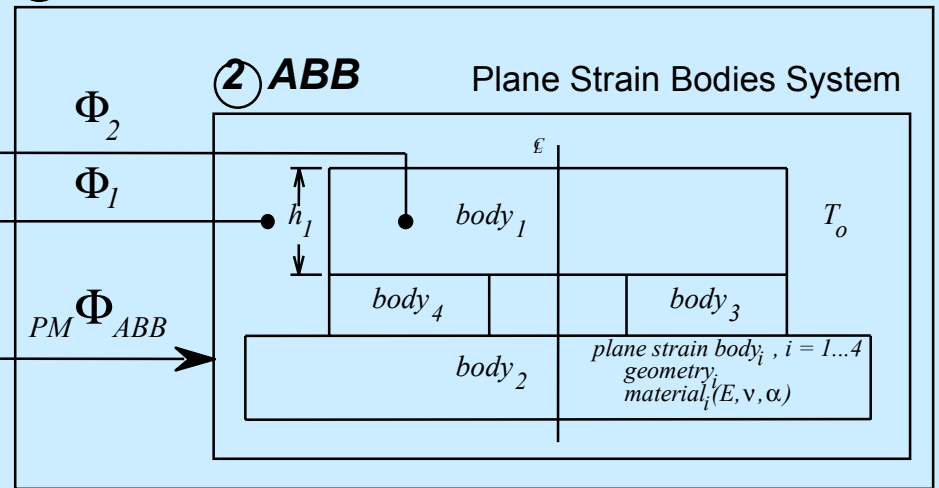
Solder Joint Deformation CBAM

Informal Associativity Mapping

③ APM PWA Component Occurrence

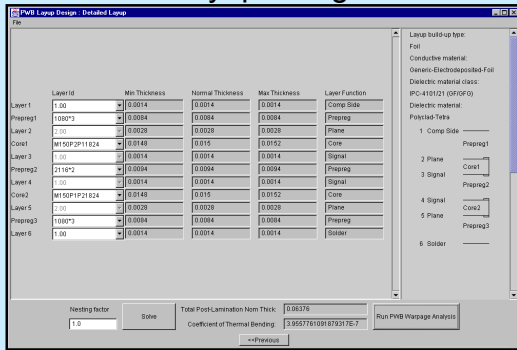


④ CBAM Component Occurrence Plane Strain Model



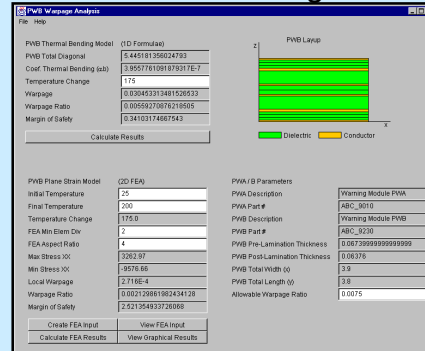
Iterative Design & Analysis

PWB Layout Design Tool



Layup Re-design

1D Thermal Bending Model



Quick Formula-based Check

$$\delta = \frac{\alpha_b L^2 \Delta T}{t}$$

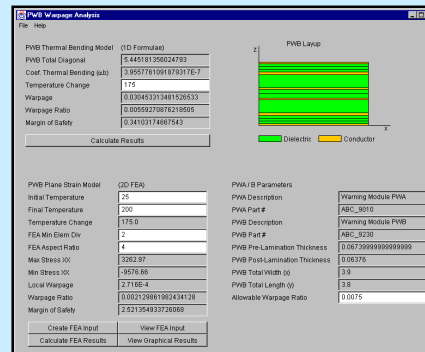
$$\alpha_b = \frac{\sum w_i \alpha_i y_i}{t / 2 \sum w_i}$$

Analyzable Product Model

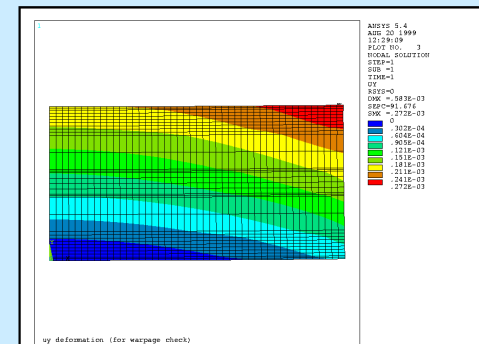
PWB Warpage Modules



2D Plane Strain Model

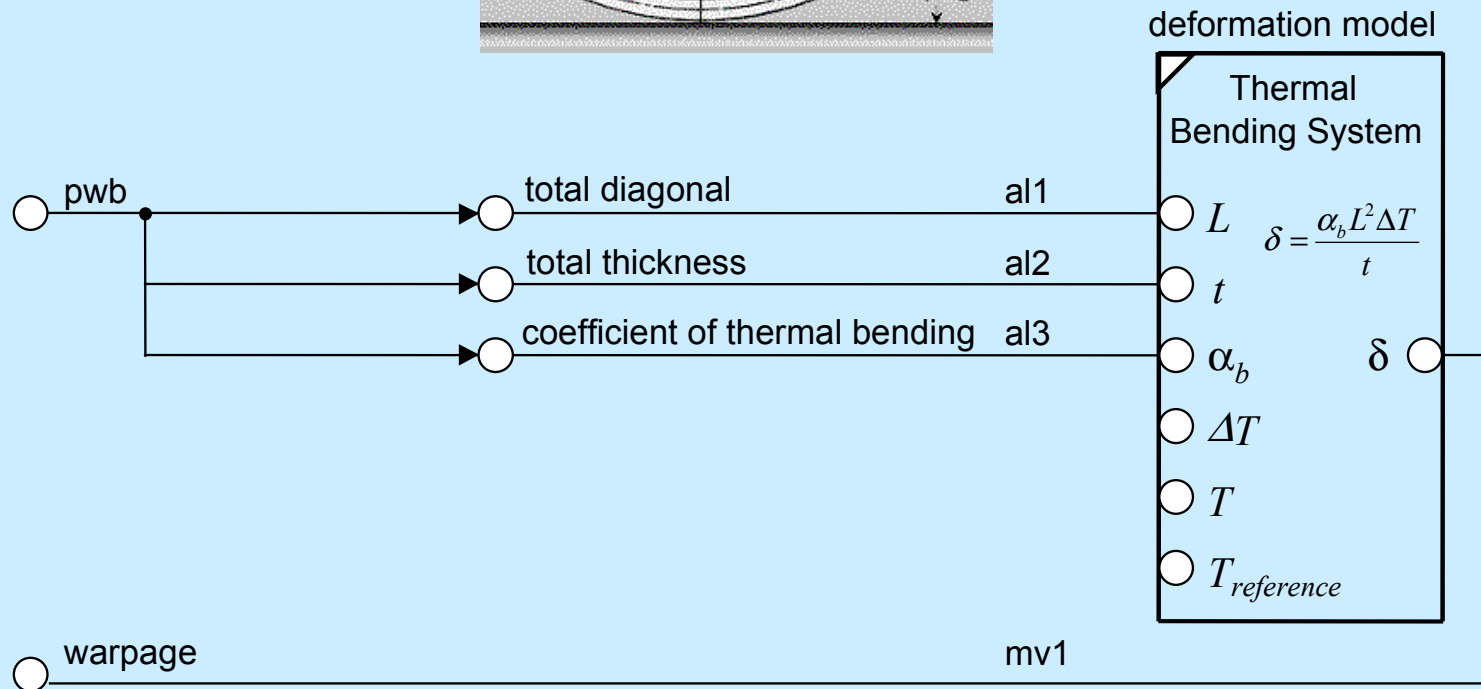
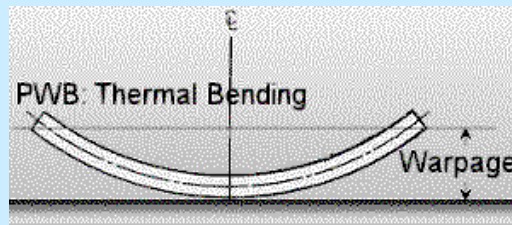


Detailed FEA Check



PWB Warpage CBAM

PWB Thermal Bending Model (1D formula-based)



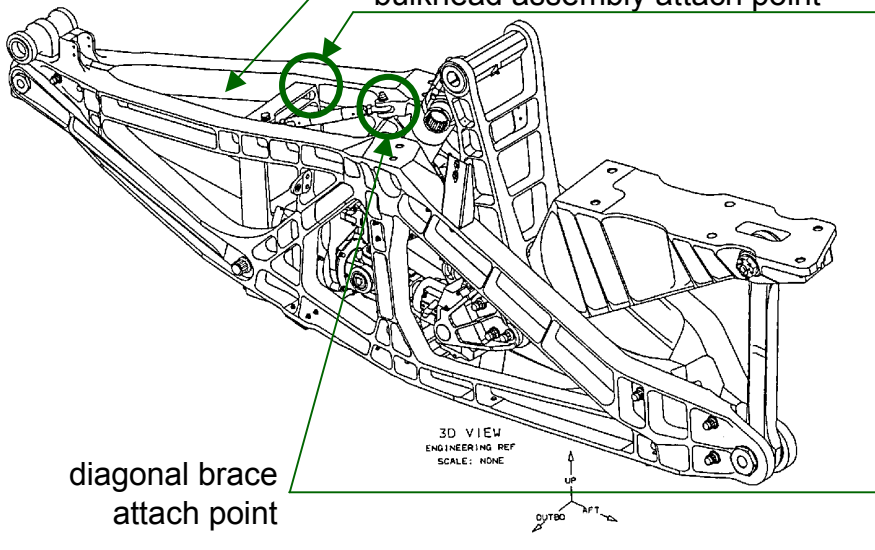
Aerospace Structural Analysis Test Case

GIT Work in Boeing PSI Project

Design Objects

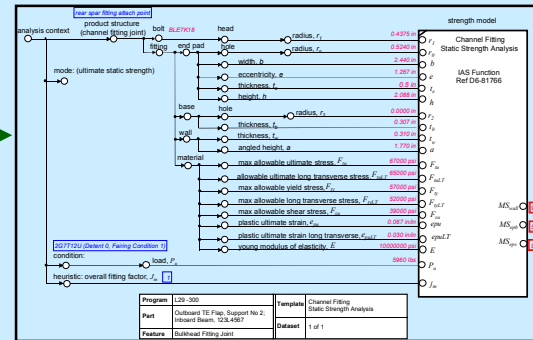
flap support assembly inboard beam (a.k.a. "bike frame")

bulkhead assembly attach point

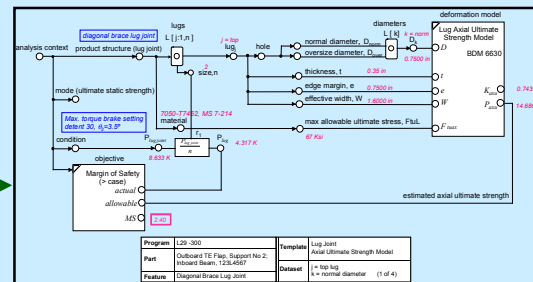


diagonal brace
attach point

Analysis Objects

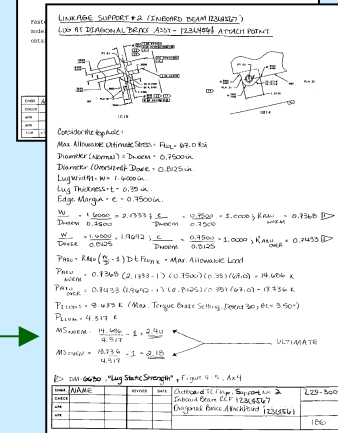
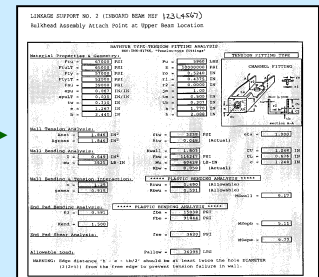


fitting analysis



lug analysis

Pullable Views



Modular, Integrated, Active, Multidirectional,
Reusable, User-Definable

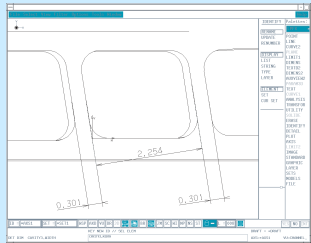
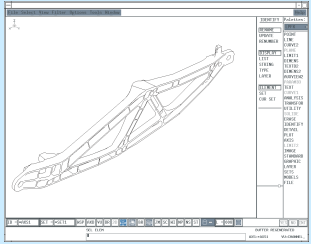
Flexible High Diversity Design-Analysis Integration

Aerospace Examples:

“Bike Frame” / Flap Support Inboard Beam

Design Tools

MCAD Tools

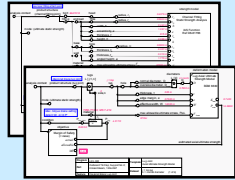


Materials DB

MATDB-like

Fasteners DB

FASTDB-like



Modular, Reusable
Template Libraries

Analysis Modules (CBAMs)
of Diverse Feature:Mode, & *Fidelity*

XaiTools

Analysis Tools

General Math

Mathematica

In-House
Codes

Analyzable
Product Model



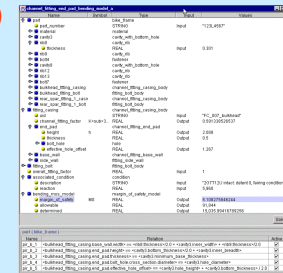
1.5D

Lug:
Axial/Oblique;
Ultimate/Shear



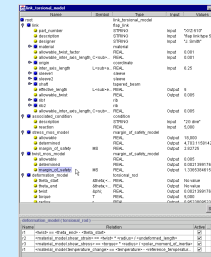
1.5D

Fitting:
Bending/Shear

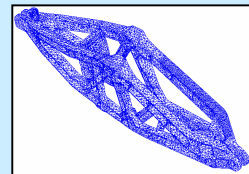


3D

Assembly:
Ultimate/
FailSafe/Fatigue*



FEA
*Elfini**



* = Item not yet available in toolkit (all others have working examples)

Today's Fitting Catalog Documentation

from DM 6-81766 Design Manual

Calculation Steps

Categories of Idealized Fittings

End Pad Analysis – Two margins of safety, one from the bending stress and one for the shear stress will be calculated. Unless otherwise noted, do not extrapolate the K_3 curves.

1. End Pad Analysis – Bending

Step 1: Compute $\frac{r_1}{h}$ and $\frac{b}{h}$.

Step 2: From FIGURE 3-3 read K_3 . If b/h is less than 1.0, use the K_3 value for b/h equal to 1.0. If r_1/h is greater than 0.4, use the K_3 value for r_1/h equal to 0.4.

Step 3: Determine the bending stress, f_{be} :

$$f_{be} = K_3 (2e - t_b) \frac{P}{h t_e^2}$$

Step 4: Determine the allowable apparent bending stress, F_b , from the plastic bending curves in the appropriate DM-4XXX using $K = 1.5$ and an actual extreme fiber stress equal to F_{lu} .

Step 5: The margin of safety is

$$M.S. = \frac{F_b}{j_m f_{be}} - 1$$

2. End Pad Analysis – Shear

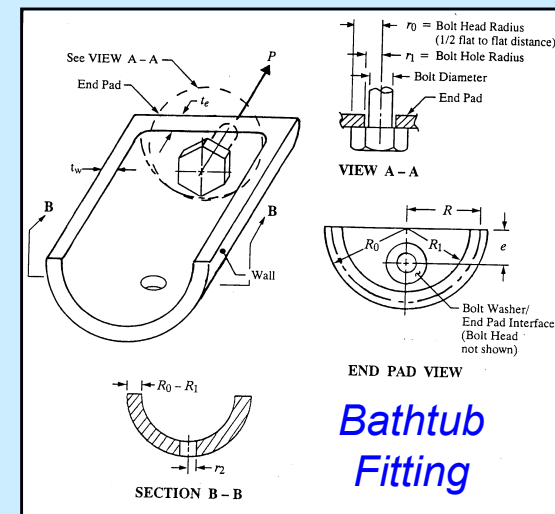
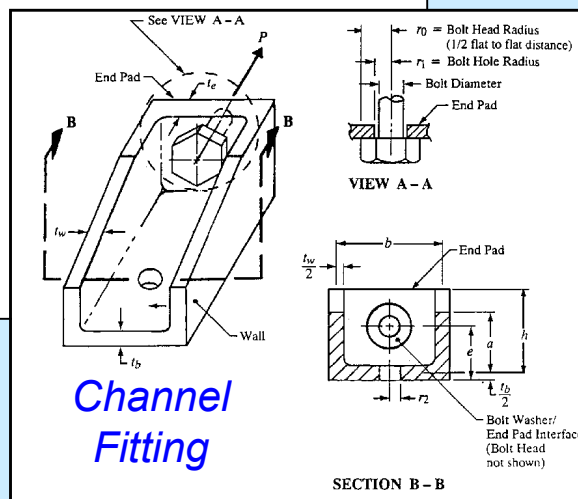
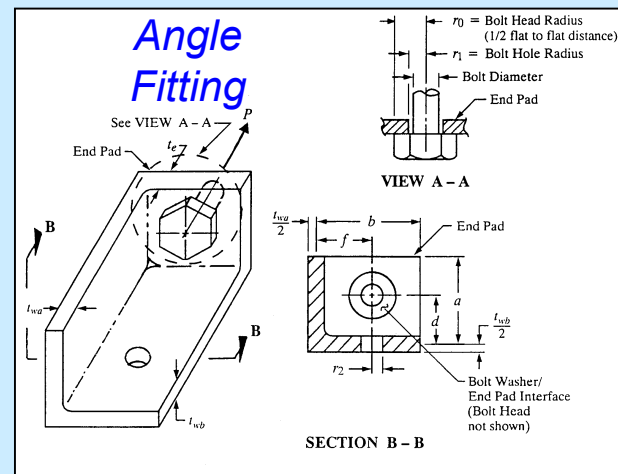
Step 1: Actual shear stress is

$$f_{se} = \frac{P}{2\pi r_0 t_e}$$

Step 2: The margin of safety is

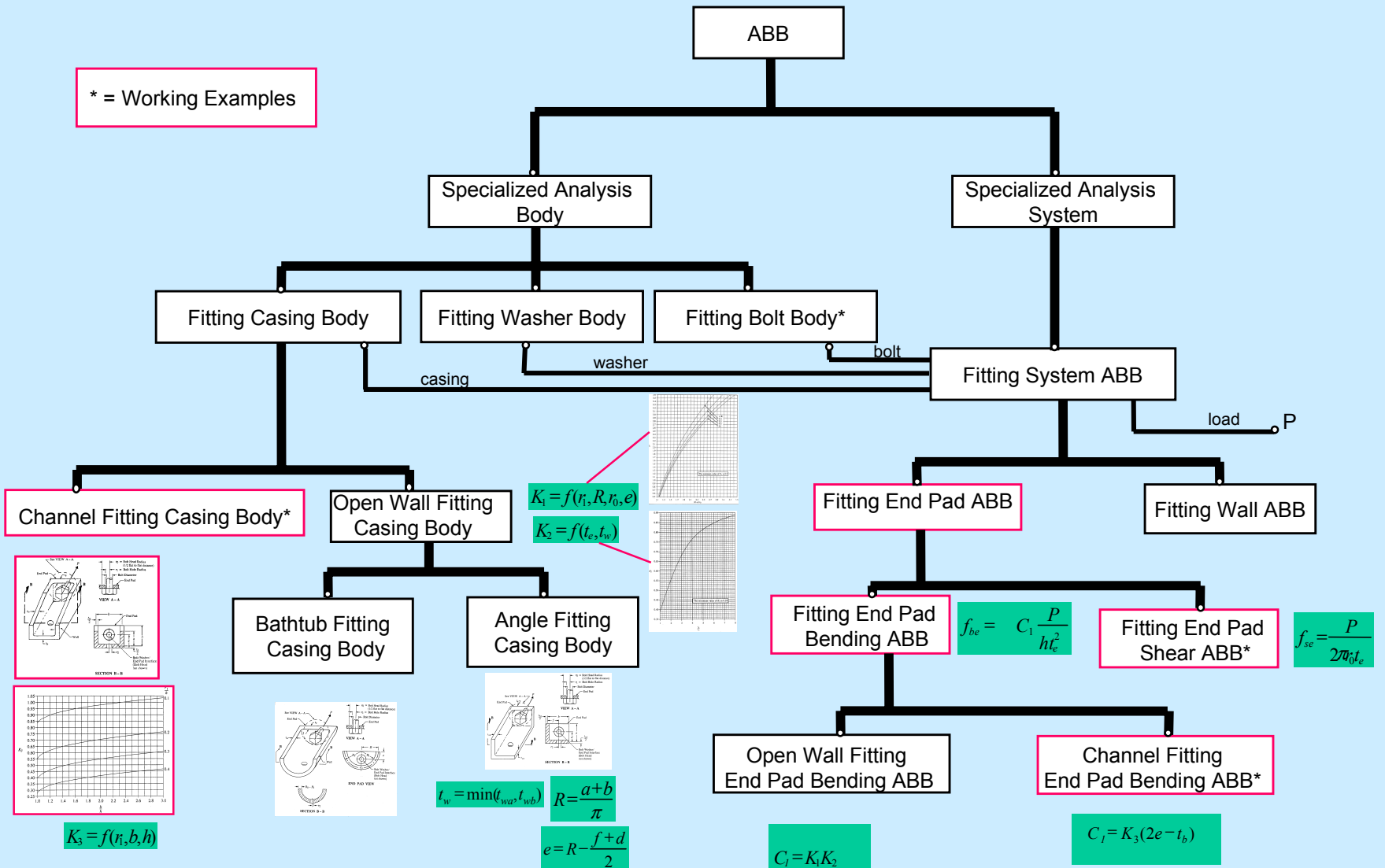
$$M.S. = \frac{F_{su}}{j_m f_{se}} - 1$$

Channel Fitting End Pad Bending Analysis

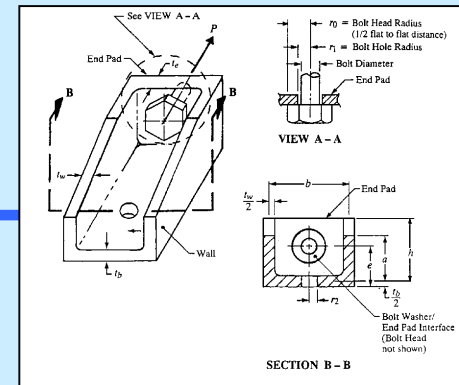


Object-Oriented Hierarchy of Fitting ABBs

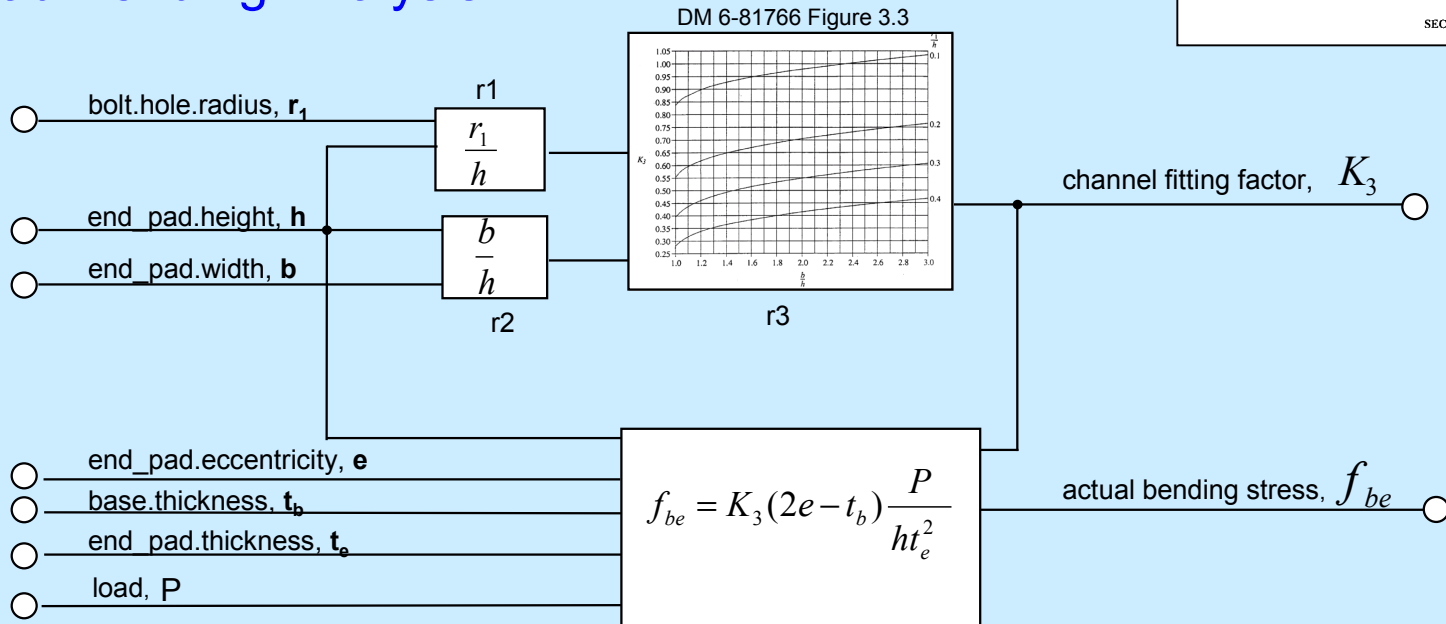
* = Working Examples



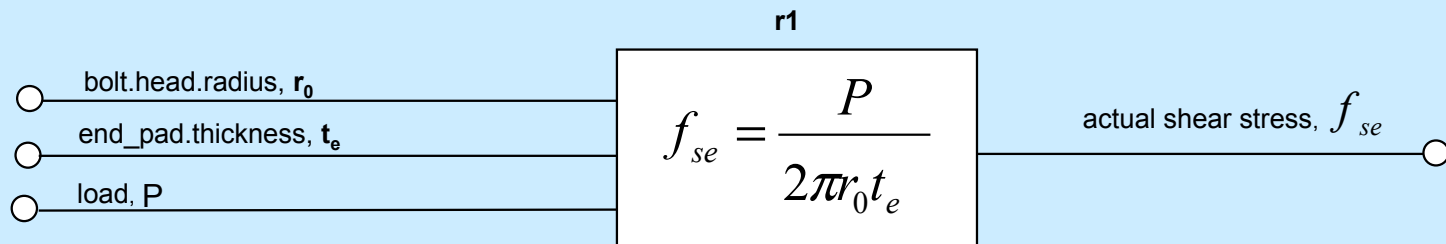
Channel Fitting System ABBs



End Pad Bending Analysis

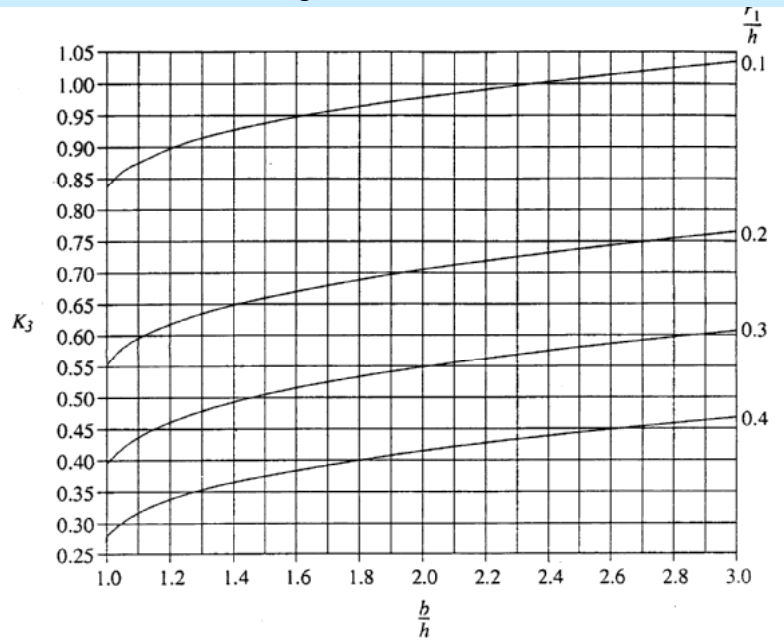


End Pad Shear Analysis

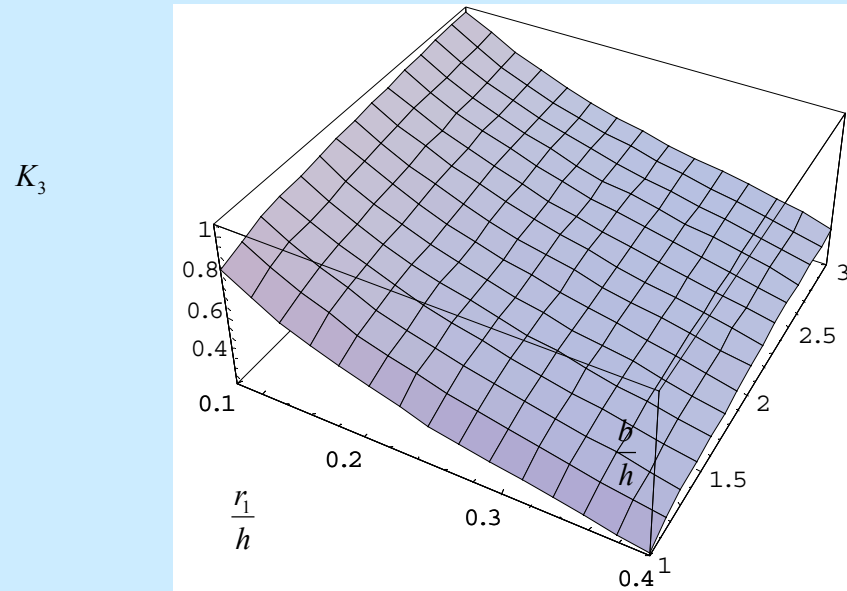


Implementation of Channel Fitting Factor, K_3 as a Reusable Relation in an External Tool

Design Manual Curves

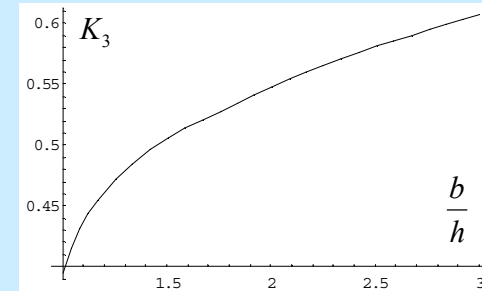
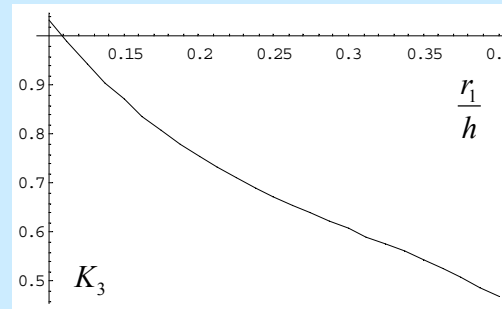


Mathematica Implementation

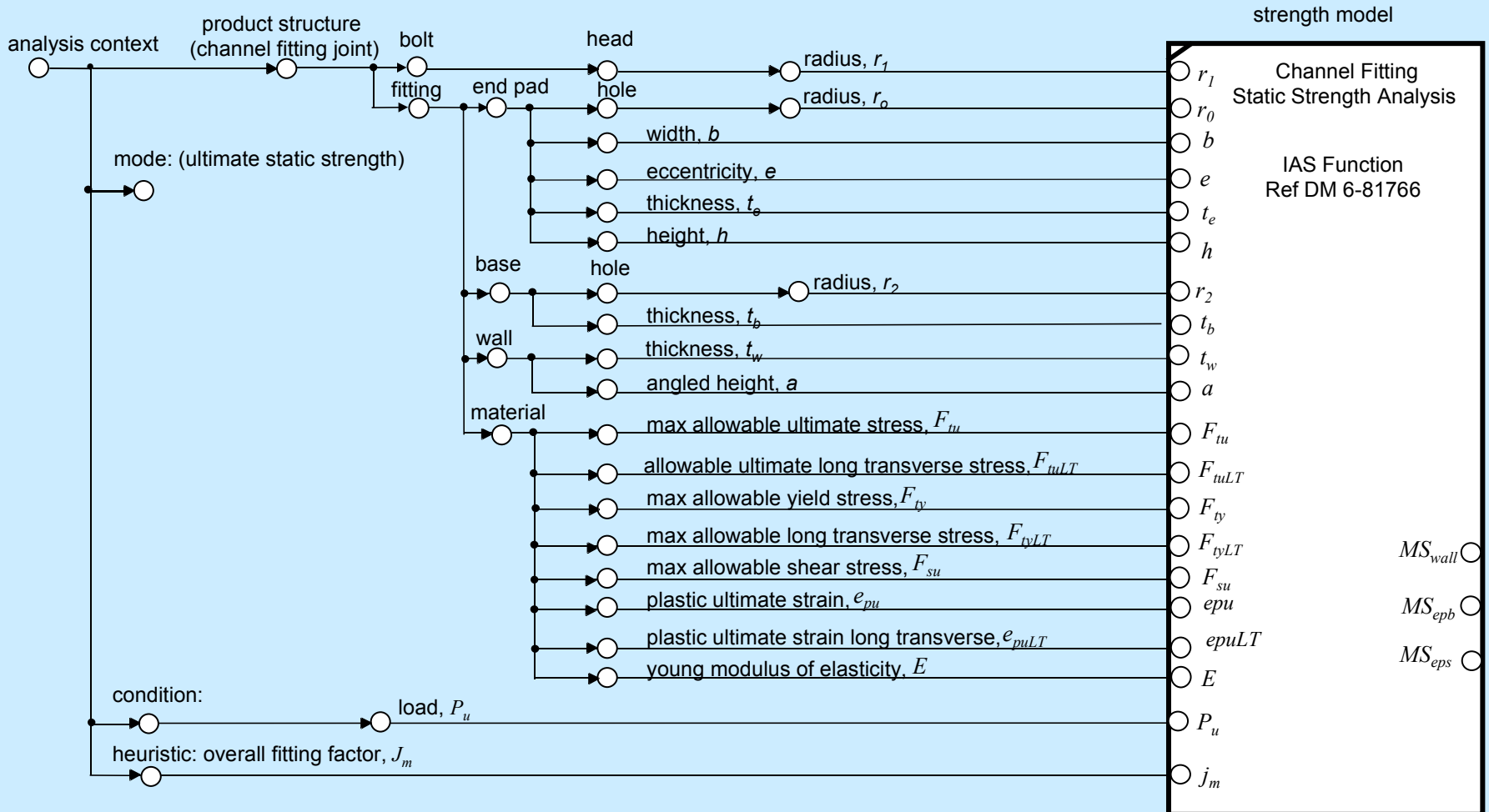


| r 1/h = 0.1 | | r 1/h = 0.2 | | r 1/h = 0.3 | | r 1/h = 0.4 | |
|-------------|--------|-------------|--------|-------------|-------|-------------|--------|
| b/h | K 3 | b/h | K 3 | b/h | K 3 | b/h | K 3 |
| 1.0 | 0.836 | 1.0 | 0.5525 | 1.0 | 0.395 | 1.0 | 0.28 |
| 1.04 | 0.8575 | 1.04 | 0.575 | 1.04 | 0.415 | 1.04 | 0.2975 |
| 1.1 | 0.8752 | 1.1 | 0.596 | 1.1 | 0.437 | 1.1 | 0.317 |
| 1.2 | 0.898 | 1.2 | 0.618 | 1.2 | 0.461 | 1.18 | 0.335 |
| 1.34 | 0.92 | 1.34 | 0.641 | 1.34 | 0.485 | 1.34 | 0.359 |
| 1.5 | 0.938 | 1.5 | 0.66 | 1.5 | 0.505 | 1.5 | 0.375 |
| 1.8 | 0.9645 | 2.0 | 0.705 | 2.02 | 0.55 | 2.0 | 0.415 |
| 2.1 | 0.985 | 2.54 | 0.74 | 2.4 | 0.575 | 2.52 | 0.445 |
| 3.0 | 1.035 | 3.0 | 0.756 | 3.0 | 0.607 | 3.0 | 0.468 |

DM 6-81766 Graph (Figure 3.3)



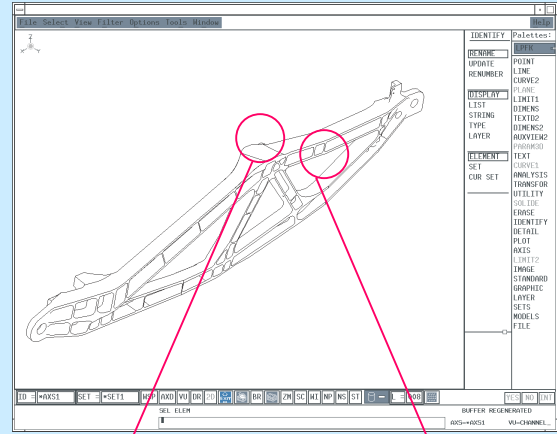
Reusable Channel Fitting Analysis Module (CBAM)



Application to an Aerospace Part

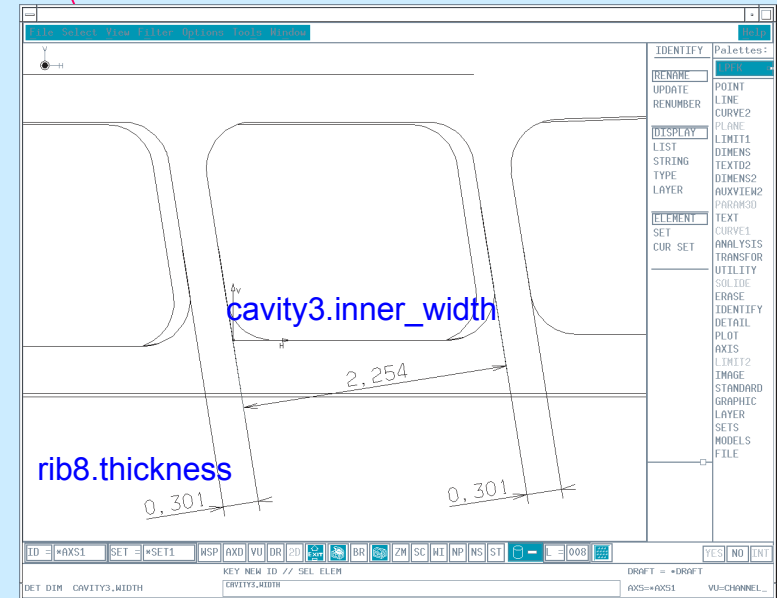
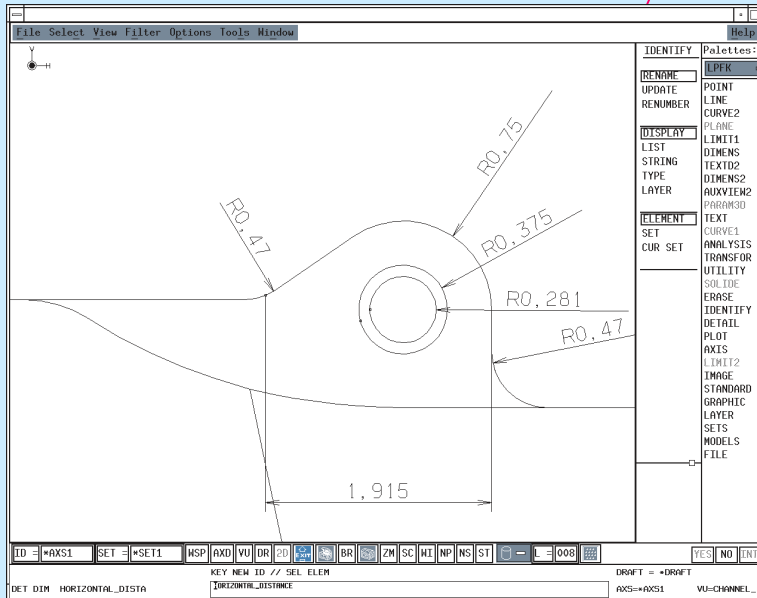
APM Associativity with Tagged CATIA Model

Bike Frame
CATIA CAD Model



Diagonal Brace Lug

Bulkhead Fitting Casing

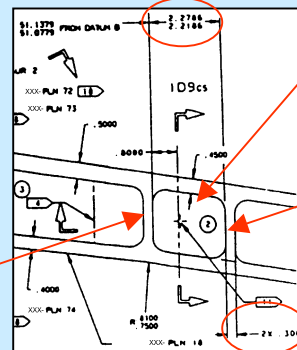
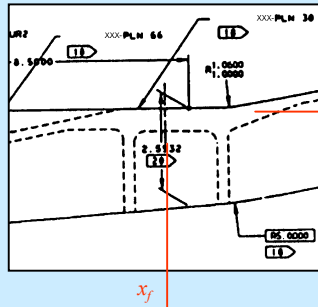
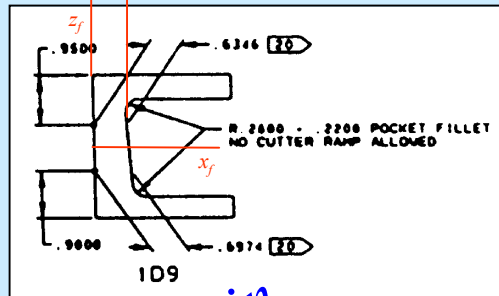


Explicit Capture of Idealizations

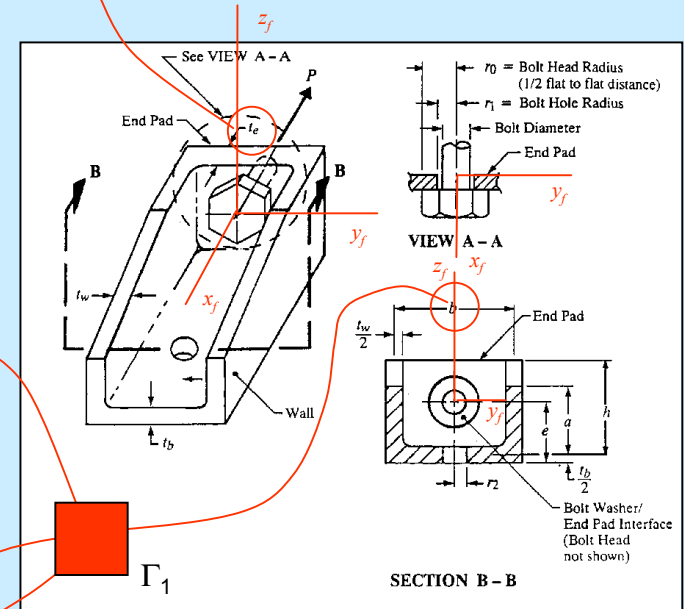
(part-specific template adaptation in bike frame case)

Features/Parameters Tagged in CAD Model (CATIA)

cavity3.base.minimum_thickness



Idealized Features



Tension Fitting Analysis

Γ_i - Relations between CAD parameters and idealized parameters

$$\Gamma_1 : b = \text{cavity3.inner_width} + \text{rib8.thickness}/2 + \text{rib9.thickness}/2$$

$$\Gamma_2 : t_e = \text{cavity3.base.minimum_thickness}$$

Missing in Today's Process

Today's Typical Fitting Analysis

Idealized CAD data manually transformed and input

Missing Design-Analysis Associativity

LINKAGE SUPPORT NO. 2 (INBOARD BEAM REF 123L4567)
Bulkhead Assembly Attach Point at Upper Beam Location

BATHTUB TYPE TENSION FITTING ANALYSIS
REF: DM6-81766, "Tension-type fittings"

| Material Properties & Geometry: | | TENSION FITTING TYPE | |
|---------------------------------|-------------|----------------------|--------------|
| Ftu = | 67000 PSI | Pu = | 5960 LBS |
| FtuLT = | 65000 PSI | E = | 10000000 PSI |
| Fty = | 57000 PSI | ro = | 0.5240 IN |
| FtyLT = | 52000 PSI | ri = | 0.4375 IN |
| Fsu = | 39000 PSI | r2 = | 0.0000 IN |
| epu = | 0.067 IN/IN | jm = | 1.00 |
| epuLT = | 0.030 IN/IN | te = | 0.500 IN |
| tw = | 0.310 IN | tb = | 0.307 IN |
| e = | 1.267 IN | a = | 1.770 IN |
| b = | 2.440 IN | h = | 2.088 IN |

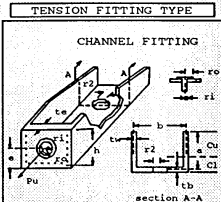


Diagram: CHANNEL FITTING, section A-A. Dimensions shown include r1, r2, jm, te, tb, a, h, b, e, and Pu.

| Wall Tension Analysis: | | Wall Bending Analysis: | |
|------------------------|-----------------------|------------------------|----------------|
| Anet = | 1.846 IN ² | ftw = | 3228 PSI |
| Agross = | 1.846 IN ² | Rtw = | 0.048 (Actual) |
| I = | 0.649 IN ⁴ | Kwall = | 1.803 |
| mu = | 3525 LB-IN | Fbw = | 116247 PSI |
| | | Mu = | 60428 LB-IN |
| | | Rbw = | 0.058 (Actual) |

| Wall Bending & Tension Interaction: | | ***** PLASTIC BENDING ANALYSIS ***** | |
|-------------------------------------|-------|--------------------------------------|-------------------|
| n = | 1.25 | Rtwu = | 0.490 (Allowable) |
| gamma = | 0.915 | Rbwu = | 0.591 (Allowable) |
| | | Mswall = | 9.17 |

| End Pad Bending Analysis: | | ***** PLASTIC BENDING ANALYSIS ***** | |
|---------------------------|-------|--------------------------------------|-----------|
| K3 = | 0.591 | fbe = | 15038 PSI |
| Kend = | 1.500 | Fbe = | 91844 PSI |
| | | Msepb = | 5.11 |

| End Pad Shear Analysis: | | ***** PLASTIC BENDING ANALYSIS ***** | |
|-------------------------|----------|--------------------------------------|------|
| fse = | 3620 PSI | Mseps = | 9.77 |

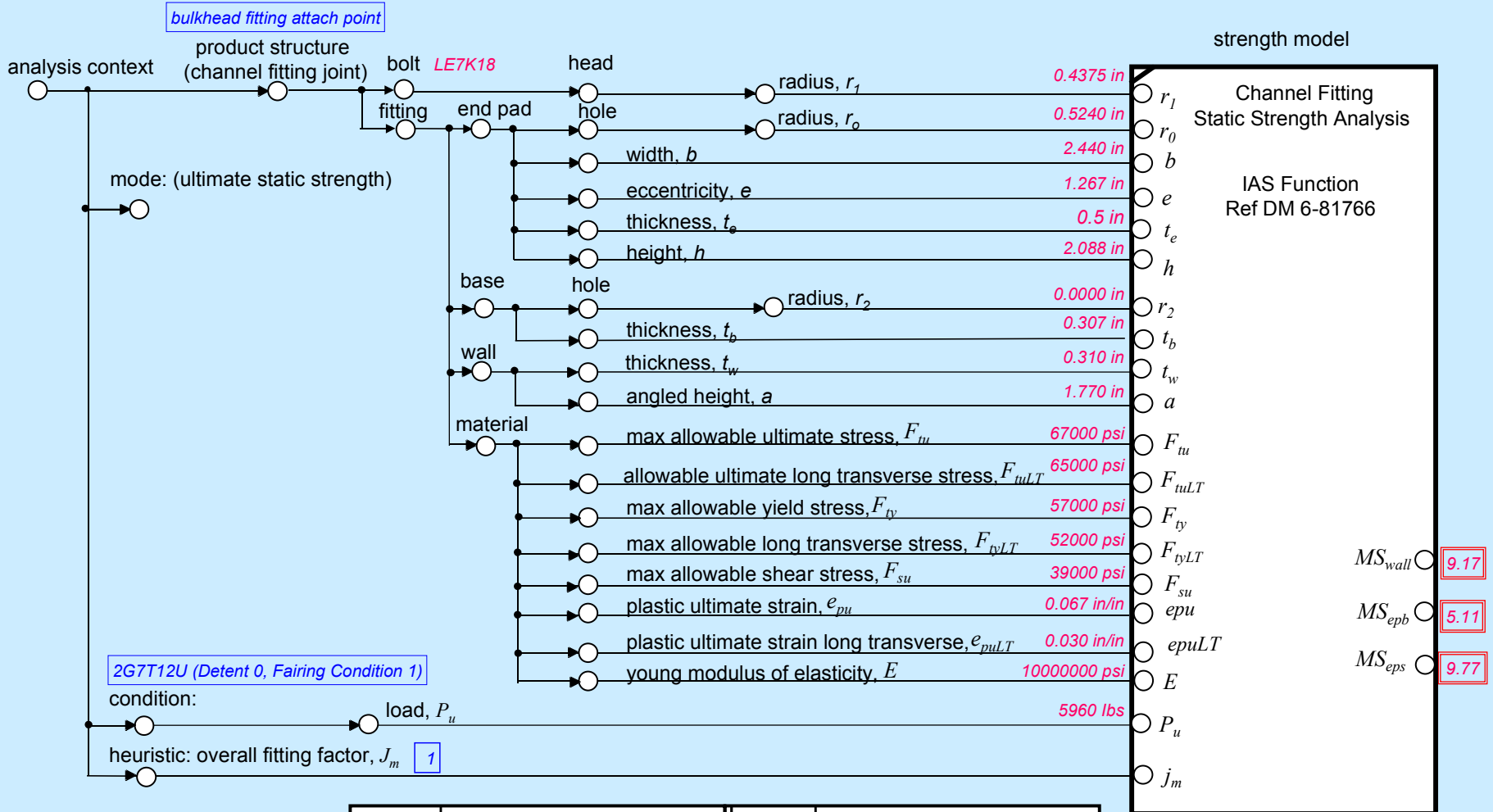
Allowable Load: Pallow = 36395 LBS

WARNING: Edge distance 'h - e - tb/2' should be at least twice the hole DIAMETER (2(2ri)) from the free edge to prevent tension failure in wall.

Fastener is LE7K18 and represented as beam element number 362 in FEA model. Load considered is 2G7T12U intact (Detent 0, Fairing Condition 1) and is obtained from the FEA model axial beam loads.

| ENGR. | NAME | 12/20/96 | REVISED | DATE | Outboard TE Flap, Support No. 2
Bulkhead Attachment Location to 123L4567
ibbulk.tem ibbulk.dta
ENGINEER DEVELOPED TEMPLATE | 029-300 |
|-------|--------------|----------|---------|------|---|----------|
| CHECK | | | | | | |
| APR | | | | | | |
| APR | | | | | | |
| FGM | 3734007-PROD | IAS | | | | PAGE 206 |

CBAM Instance for Channel Fitting Analysis



| | | | |
|----------------|--|-----------------|--|
| Program | L29 -300 | Template | Channel Fitting Static Strength Analysis |
| Part | Outboard TE Flap, Support No 2; Inboard Beam, 123L4567 | Dataset | 1 of 1 |
| Feature | Bulkhead Fitting Joint | | |

Bike Frame Bulkhead Fitting Analysis Using COB-based Templates

| Name | Symbol | Type | Input | Values |
|----------------------------|------------------|-----------------------------|--------|---|
| part | | bike_frame | | |
| part_number | | STRING | Input | "123L4567" |
| material | | material | | |
| cavity3 | | cavity_with_bottom_hole | | |
| rib8 | | cavity_rib | | |
| thickness | | REAL | Input | 0.301 |
| rib9 | | cavity_rib | | |
| bolt4 | | fastener | | |
| cavity9 | | cavity_with_bottom_hole | | |
| rib12 | | cavity_rib | | |
| rib13 | | cavity_rib | | |
| bolt7 | | fastener | | |
| bulkhead_fitting_casing | | channel_fitting_casing_body | | |
| bulkhead_fitting_bolt | | fitting_bolt_body | | |
| rear_spar_fitting_1_casing | | channel_fitting_casing_body | | |
| rear_spar_fitting_1_bolt | | fitting_bolt_body | | |
| fitting_casing | | channel_fitting_casing_body | | |
| uid | | STRING | Input | "FC_007_bulkhead" |
| channel_fitting_factor | K₃... | REAL | Output | 0.591338526537 |
| end_pad | | channel_fitting_end_pad | | |
| height | h | REAL | Output | 2.088 |
| thickness | | REAL | Output | 0.5 |
| bolt_hole | | hole | | |
| effective_hole_offset | | REAL | Output | 1.267 |
| base_wall | | channel_fitting_base_wall | | |
| side_wall | | fitting_side_wall | | |
| fitting_bolt | | fitting_bolt_body | | |
| overall_fitting_factor | | REAL | Input | 1 |
| associated_condition | | condition | | |
| description | | STRING | Input | "2G7T12U intact: detent 0, fairing condition 1" |
| reaction | | REAL | Input | 5,960 |
| bending_mos_model | | margin_of_safety_model | | |
| margin_of_safety | MS | REAL | Output | 5.108275846244 |
| allowable | | REAL | Output | 91,844 |
| determined | | REAL | Output | 15,035.99416789256 |

| Name | Relation | Active |
|---------|---|-------------------------------------|
| pir_b_1 | <bulkhead_fitting_casing.base_wall.width> == <rib8.thickness>/2.0 + <cavity3.inner_width> + <rib9.thickness>/2.0 | <input checked="" type="checkbox"/> |
| pir_b_2 | <bulkhead_fitting_casing.end_pad.height> == <cavity3.bottom_thickness>/2.0 + <cavity3.inner_breadth> | <input checked="" type="checkbox"/> |
| pir_b_3 | <bulkhead_fitting_casing.end_pad.thickness> == <cavity3.minimum_base_thickness> | <input checked="" type="checkbox"/> |
| pir_b_4 | <bulkhead_fitting_casing.end_pad.bolt_hole.cross_section.diameter> == <cavity3.hole_diameter> | <input checked="" type="checkbox"/> |
| pir_b_5 | <bulkhead_fitting_casing.end_pad.effective_hole_offset> == <cavity3.hole_height> + <cavity3.bottom_thickness> / 2.0 | <input checked="" type="checkbox"/> |

Detailed CAD data from CATIA

Library data for materials & fasteners

Idealized analysis features in APM

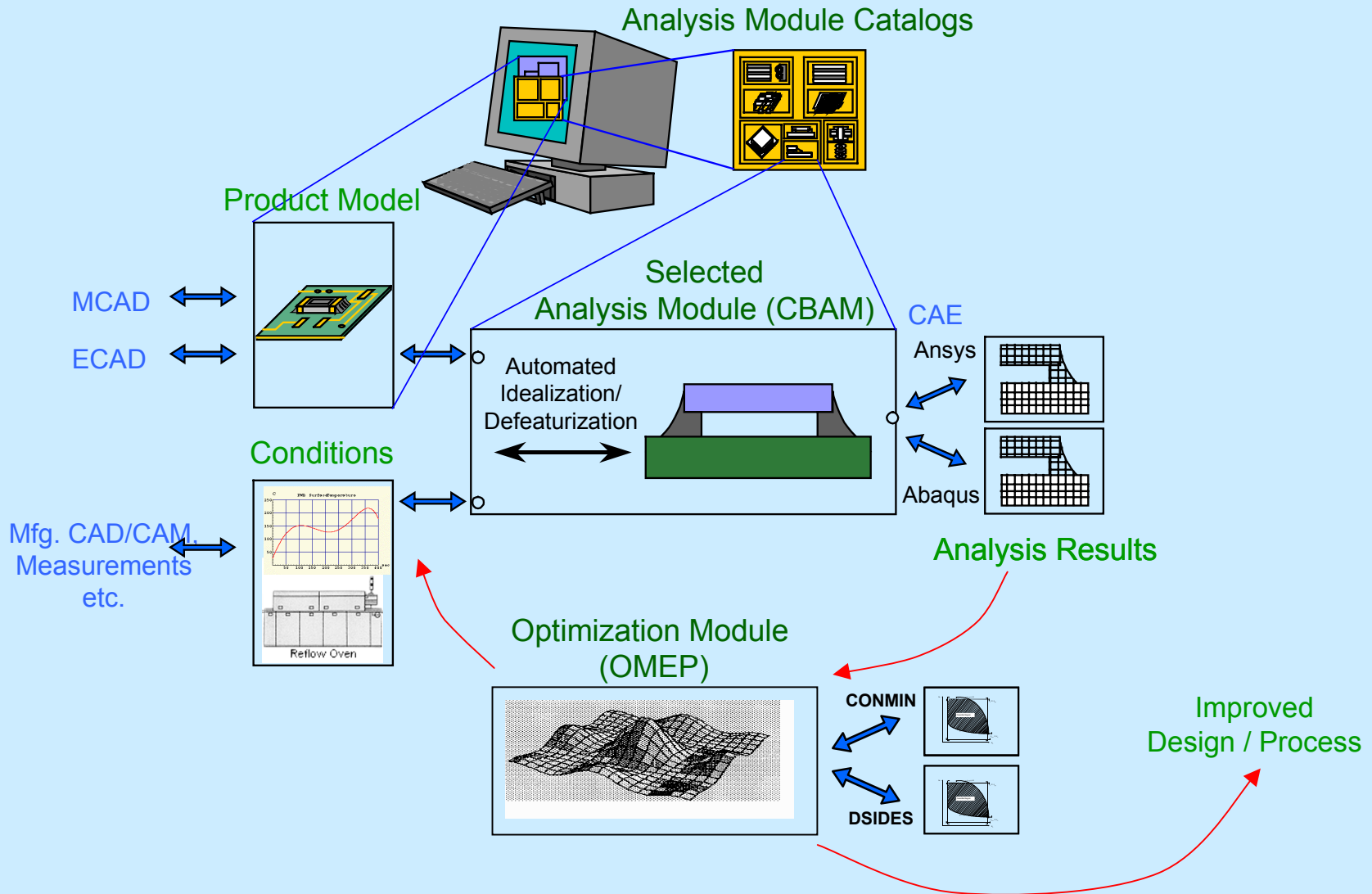
Fitting & MoS ABBs

Explicit multi-directional associativity between detailed CAD data & idealized analysis features

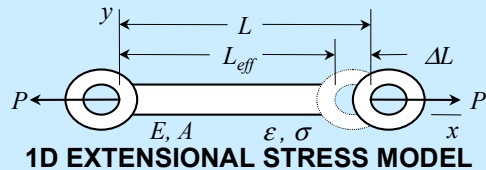
Outline

- ◆ Analysis Integration Challenges
- ◆ Introduction to Constrained Objects (COBs)
- ◆ Overview of COB-based XAI
- ◆ Example Applications
 - ◆ Electronic Packaging Thermomechanical Analysis
 - ◆ Aerospace Structural Analysis
- ◆ Optimization Integration ←
- ◆ Summary

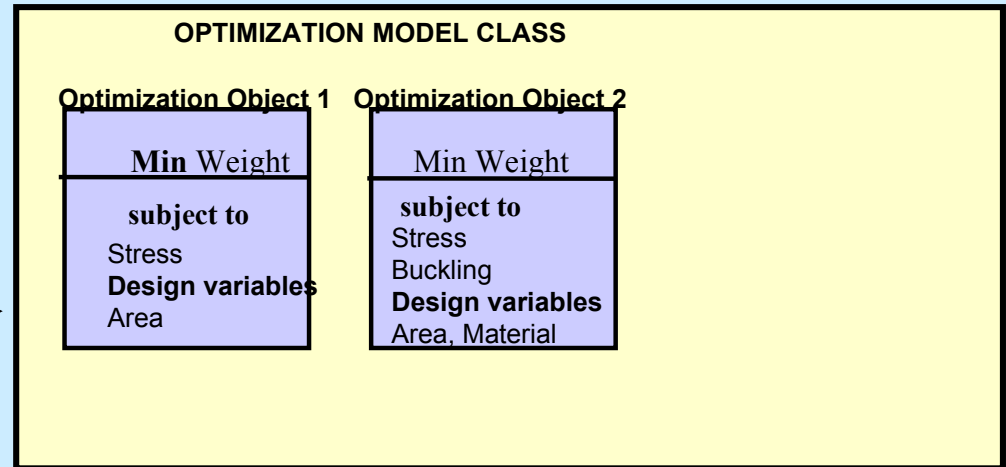
Optimization Integration Thrust (work-in-process)



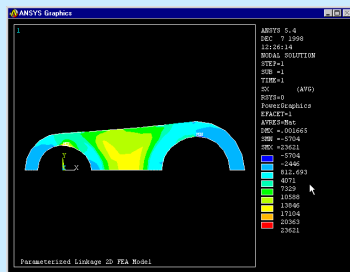
Optimization Model Diversity



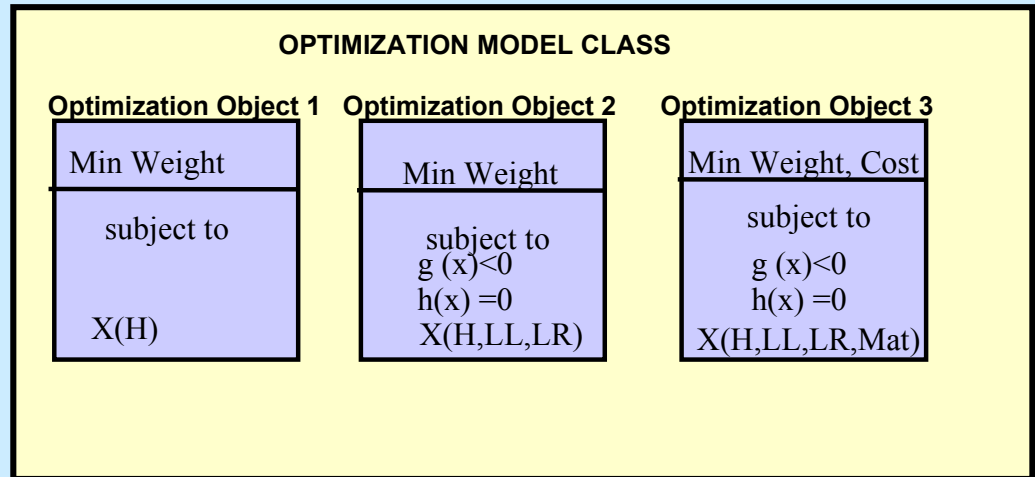
Analysis Model(s)
Enhancement and/or Addition



Objective, design variable, and/or constraint function enhancement



2D PLANE STRAIN MODEL



Optimization Model Enhancement

OPTIMIZATION MODEL I

Minimize

$$f_1 = \rho LA \quad \text{Weight}$$

Subject to

$$g_1 = MS_{stress}(A) \geq 0 \quad \text{Normal Stress Margin of Safety}$$

Design variables

$$\mathbf{X} = \{A\}$$

OPTIMIZATION MODEL II

Minimize

$$f_1 = \rho LA \quad \text{Weight}$$

Subject to

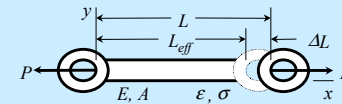
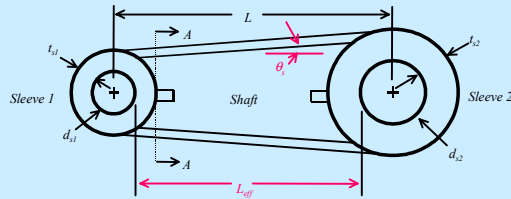
$$g_1 = MS_{stress}(A) \geq 0 \quad \text{Normal Stress Margin of Safety}$$

Design variables

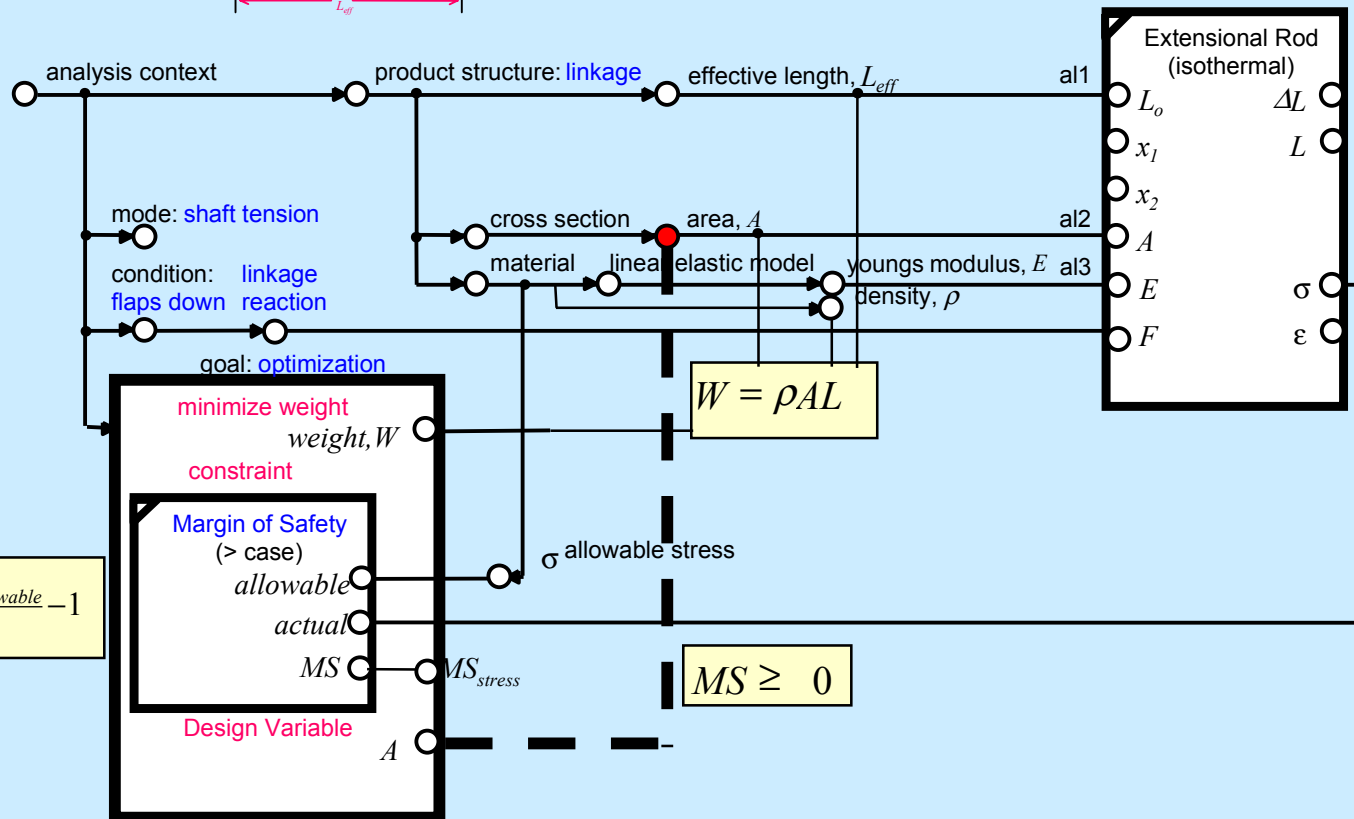
$$\mathbf{X} = \{A, \text{material}\}$$

Minimization of Weight of a Linkage

X(area) subject to (extensional stress)



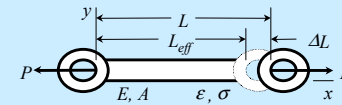
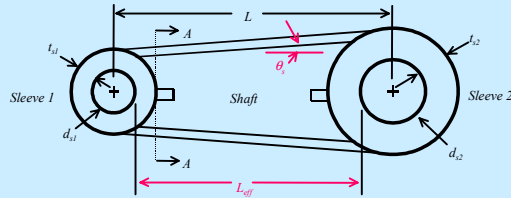
deformation model



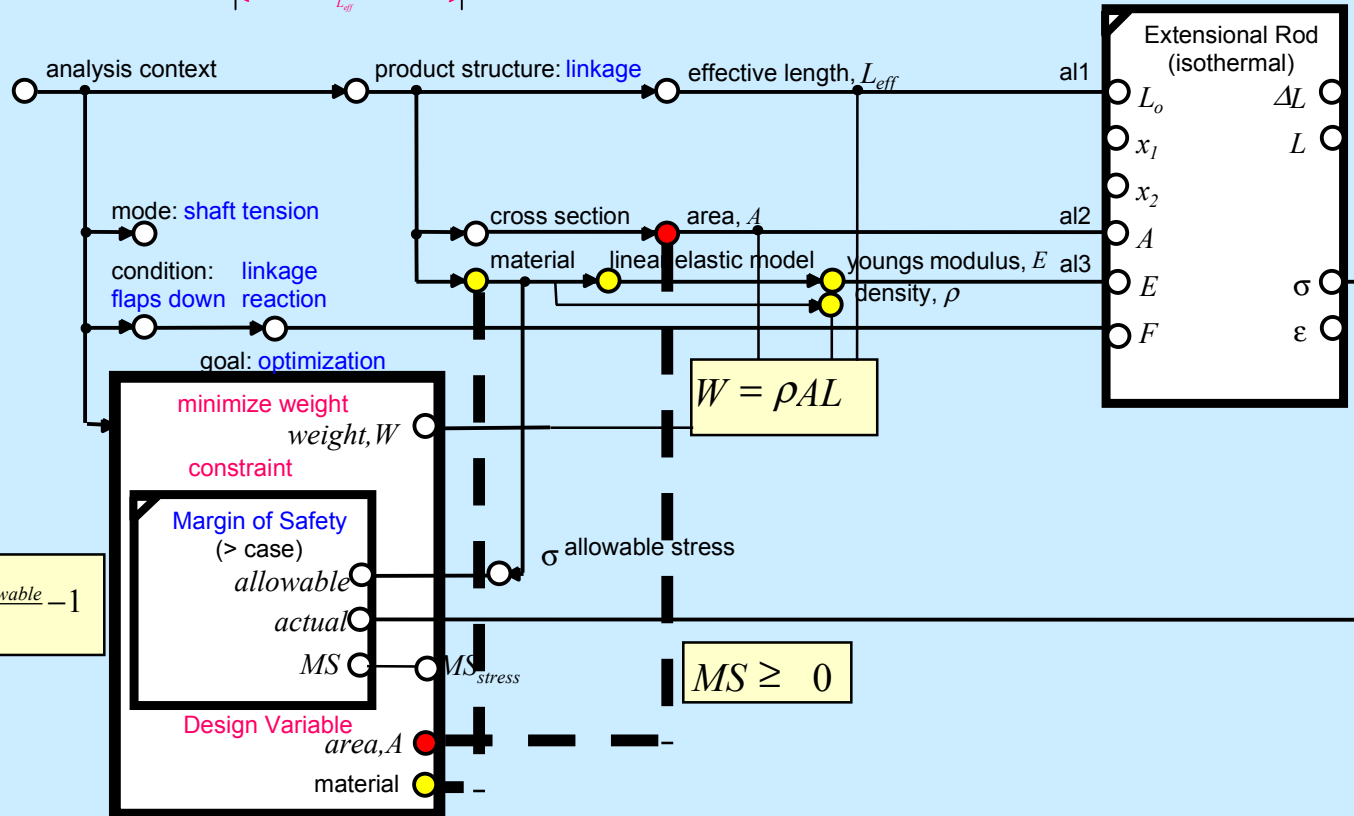
$$MS_{stress} = \frac{\sigma_{allowable}}{\sigma} - 1$$

Minimization of Weight of a Linkage

X(area, material) subject to (extensional stress)



deformation model



$$MS_{stress} = \frac{\sigma_{allowable}}{\sigma} - 1$$

Optimization Model Enhancement

OPTIMIZATION MODEL III

Minimize

$$f_1 = \rho LA \quad \text{Weight}$$

Subject to

$$g_1 = MS_{stress}(A) \geq 0 \quad \text{Normal Stress Margin of Safety}$$

$$g_2 = MS_{buckling}(A) \geq 0 \quad \text{Buckling Margin of Safety}$$

Design variables

$$\mathbf{X} = \{A\}$$

OPTIMIZATION MODEL IV

Minimize

$$f_1 = \rho LA \quad \text{Weight}$$

Subject to

$$g_1 = MS_{stress}(A) \geq 0 \quad \text{Normal Stress Margin of Safety}$$

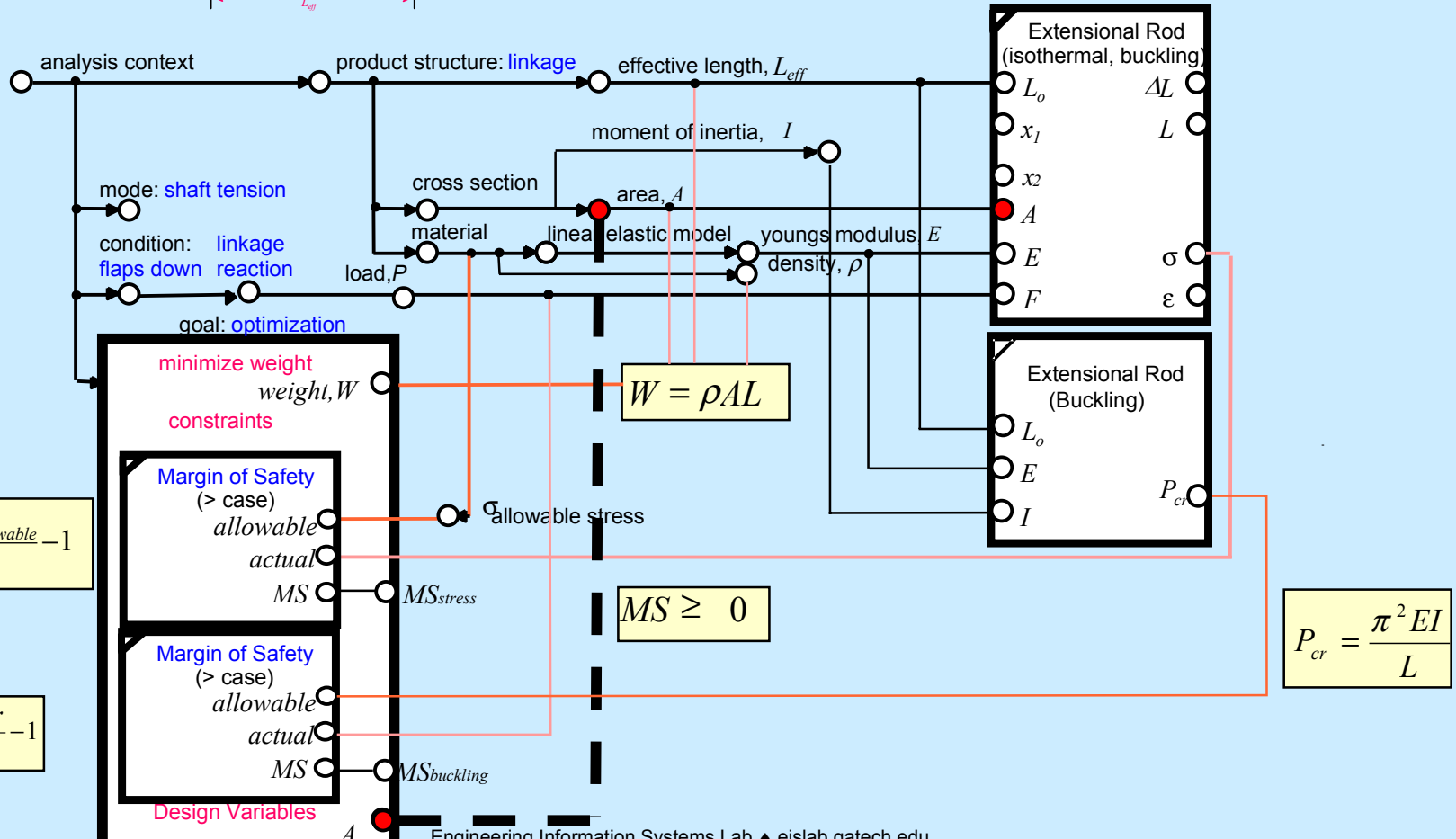
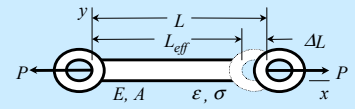
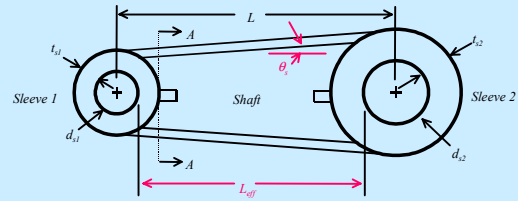
$$g_2 = MS_{buckling}(A) \geq 0 \quad \text{Buckling Margin of Safety}$$

Design variables

$$\mathbf{X} = \{A, \text{material}\}$$

Minimization of Weight of a Linkage

X(area) subject to (extensional stress, buckling load)



$$MS_{stress} = \frac{\sigma_{allowable}}{\sigma} - 1$$

$$MS_{buckling} = \frac{P_{cr}}{F} - 1$$

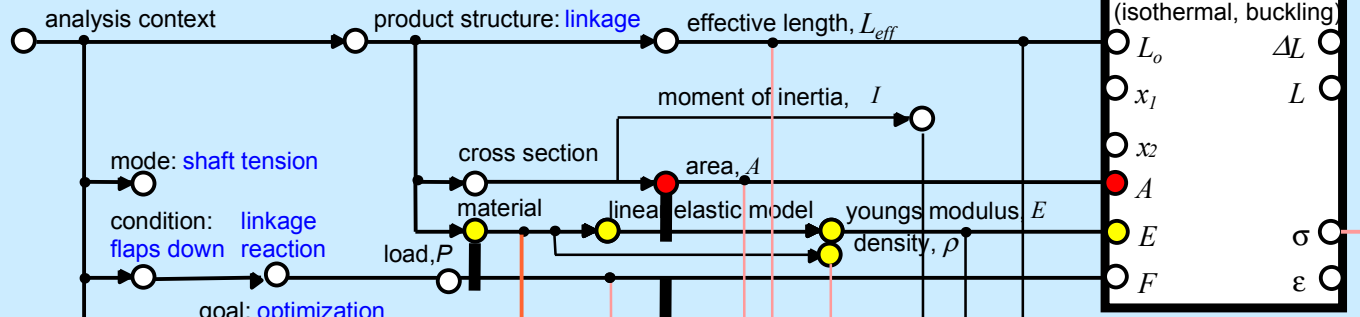
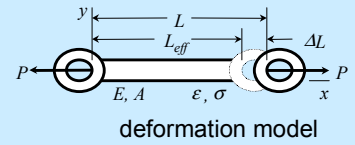
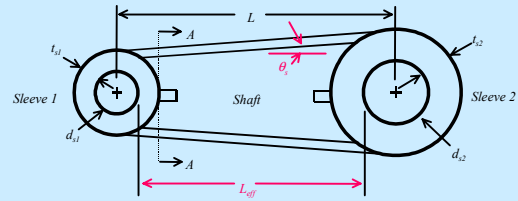
$$W = \rho AL$$

$$MS \geq 0$$

$$P_{cr} = \frac{\pi^2 EI}{L}$$

Minimization of Weight of a Linkage

X(area, material) subject to (extensional stress, buckling load)



| Extensional Rod (isothermal, buckling) | |
|--|------------|
| L_o | ΔL |
| x_1 | L |
| x_2 | |
| A | |
| E | σ |
| F | ϵ |

| Extensional Rod (Buckling) | |
|----------------------------|----------|
| L_o | |
| E | |
| I | P_{cr} |

minimize weight
weight, W

constraints

Margin of Safety (> case)
allowable
actual
 MS

Margin of Safety (> case)
allowable
actual
 MS

Design Variables A

$$W = \rho AL$$


$$MS \geq 0$$

$$P_{cr} = \frac{\pi^2 EI}{L}$$

$$MS_{stress} = \frac{\sigma_{allowable}}{\sigma} - 1$$

$$MS_{buckling} = \frac{P_{cr}}{F} - 1$$

Outline

- ◆ Analysis Integration Challenges
- ◆ Introduction to Constrained Objects (COBs)
- ◆ Overview of COB-based XAI
- ◆ Example Applications
 - ◆ Electronic Packaging Thermomechanical Analysis
 - ◆ Aerospace Structural Analysis
- ◆ Optimization Integration
- ◆ Summary 

Analysis Integration Summary

- ◆ Strong emphasis on X-analysis integration (XAI/DAI)
- ◆ Multi-Representation Architecture (MRA)
 - Addressing fundamental XAI/DAI issues
 - General methodology --> Flexibility & broad application
- ◆ Relevant project experience and research advances
 - Product data-driven analysis (STEP AP210, GenCAM, etc.)
 - Engineering service bureau (ESB) techniques
 - Object techniques for next generation aerospace analysis systems
- ◆ Tools and development services
 - Analysis integration toolkit: *XaiTools*
 - Pilot commercial ESB: U-Engineer.com
 - Company-tailored engineering information system solutions
- ◆ Industry & government collaboration

For Further Information ...

- ◆ EIS Lab web site: <http://eislabs.gatech.edu/>
 - Publications, project overviews, tools, etc.
 - See Publications, DAI/XAI, Suggested Starting Points
- ◆ *XaiTools* home page: <http://eislabs.gatech.edu/>
- ◆ Pilot commercial ESB: <http://www.u-engineer.com/>
 - Internet-based self-serve analysis
 - Analysis module catalog for electronic packaging
 - Highly automated front-ends to general FEA & math tools